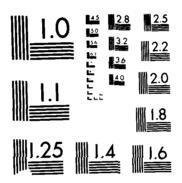
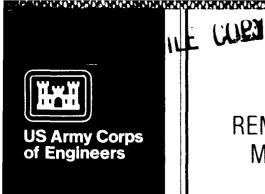
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# REMEDIAL INVESTIGATION OF CONTAMINANT MOBILITY AT NAVAL WEAPONS STATION CONCORD, CALIFORNIA

SUBTITLE APPENDIX 2.5 — 1986/87 DATA

by

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Environmental Laboratory

DEPARTMENT OF THE ARMY Waterways Experiment Station, Corps of Engineers PO Box 631, Vicksburg, Mississippi 39180-0631



June 1988 Final Report

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Prepared for DEPARTMENT OF THE NAVY

Naval Facilities Engineering Command, Western Division

San Bruno, California 94066

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11. TITL <b>E (Include Security Classification)</b> Remedial Investigation of Contaminant Mobility at Naval Weapons Station, Concord, California; Subtitle Appendix 2.5 - 1986/87 Data							
12. PERSONAL AUTHOR(S) Lee, Charles R.: O'Neil, L. Jean: Brandon, Dennis I. Bhett, Bichard C.							
12 PERSONAL AUTHOR(S) Lee, Charles R.; O'Neil, L. Jean; Brandon, Dennis L.; Rhett, Richard G. Skogerboe, John G.; Portzer, A. Susan; Price, Richard A.							
13a. TYPE OF REPORT 13b. TIME COVERED 14. DATE OF REPORT (Year, Month, Day) 15. PAGE COUNT Final report FROM 10 June 1988 121							
16. SUPPLEMENTARY NOTATION							
Available from National Technical Information Service, 5285 Port Royal Road, Springfield, VA 22161.							
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8a. NAME OF FUDNING/SPONSORING ORGANIZATION (Continued).

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18. SUBJECT TERMS (Continued).

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#### **PREFACE**

This report is an appendix to Miscellaneous Paper EL-86-2. It contains corrections and supplemental information to the original report, as well as data collected between June 1986 and August 1987.

This study was conducted by Dr. C. R. Lee, Soil Scientist, under the general supervision of Lloyd Saunders, Chief, Contaminant Mobility and Regulatory Criteria Group; Mr. D. L. Robey, Chief, Ecosystem Research and Simulation Division; Dr. C. Kirby, Chief, Environmental Resources Division; and Dr. J. Harrison, Chief, Environmental Laboratory.

Technical contributions in the conduct of field sampling, laboratory testing, and report preparation were received from the following scientists: Mr. D. L. Brandon, Statistician, for experimental design, chain of custody labeling and data analysis; Dr. J. Simmers, Research Biologist, Mr. R. G. Rhett, Biologist, and Ms. A. S. Portzer, Biologist, for the clam bioassay and condition index; Mr. J. G. Skogerboe, Hydrologist, and Mr. R. A. Price, Agronomist, for soil sample collection, surveying sample-site locations and map preparation; Ms. L. J. O'Neil, Ecologist, Mr. C. J. Newling, Wildlife Biologist, and Mr. R. Theriot, Biologist, for the wetland delineation; Mr. G. Warren, Chemist, and Mr. D. Brown, Chemist, for metal analysis of soil and animal samples. Soil samples were also analyzed by Princeton Testing Laboratory, Inc., Princeton, New Jersey. Ground-water samples were analyzed by Sequoia Analytical Laboratory, Redwood City, California. Additional assistance in manuscript preparation was received from Ms. S. Calvin, Ms. M. J. Spivey, Ms. J. Moore, and Mr. P. Laible.

Col Dwayne G. Lee, CE, was the Commander and Director of WES. Dr. Robert W. Whalin was Technical Director.

This report should be cited as follows:

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Lee, C. R., et al. 1988. "Remedial Investigation of Contaminant Mobility at Naval Weapons Station, Concord, California; Subtitle Appendix 2.5 - 1986/87 Data," Miscellaneous Paper EL-86-2, US Army Engineer Waterways Experiment Station, Vicksburg, Miss.

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#### SUBTITLE APPENDIX 2.5 - 1986/87 DATA

#### 2.5.1 Introduction

Additional investigation was conducted after publication of the Remedial Investigation (R.I.) by Lee et al. (1986), to further define the extent of contamination at Naval Weapons Station (NWS), Concord, California. The discovery of possible burial of debris at the Kiln Site required an expanded remedial investigation for that site. This report is a detailed description of these and other data collection efforts. The purposes of the report to:

- a. Provide corrections, supplemental information and clarification of the initial R.I. report.
- b. Report and evaluate additional data collected after the publication of the R.I.
- c. Assess possible effects of the 1986 flood on redistribution of contamination.
- d. Further delineate the extent of contamination in specific locations at NWS Concord.

Data are presented in Tables 2.5-A1-A32, B1-B7, C1-C10, and D1-D16. These data were derived using a nitric acid soil digestion procedure, the wet extraction procedure of the California Department of Health Sciences, the extraction procedure of the Resource Conservation and Recovery Act (RCRA), and a nitric acid tissue digestion procedure, respectively. The analytical work was performed by the Analytical Laboratory Group, Environmental Laboratory, US Army Engineer Waterways Experiment Station (WES) and Princeton Testing Laboratory, Inc., Princeton, New Jersey. Ground-water data and wetland delineation techniques were used to further evaluate the sites. Tables 2.5-D14 and D16 list ground-water data. This analytical work was performed by Sequoia Analytical Laboratory, Redwood City, California. Table 2.5-E1 lists the survey measurements of new locations.

The documents listed below are primary sources of information. Other reference documents cited in the text are listed in Section 2.5.9.

- a. Harvey and Stanley Associates, Inc. 1986. "Background Information for Section 7 Consultation at Concord Naval Weapons Station," Alviso, Calif.
- b. Lee, C. R., et al. 1986. "Remedial Investigation of Contaminant Mobility at Naval Weapons Station, Concord, California," Miscellaneous Paper EL-86-2, US Army Engineer Waterways Experiment Station, Vicksburg, Miss.
- c. Lee, C. R., Cullinane, M. John Jr., and O'Neil, L. Jean. 1988. "Feasibility Study of Contamination Remediation at Naval Weapons Station, Concord, California; Volume III: Figures," Miscellaneous Paper EL-86-3, US Army Engineer Waterways Experiment Station, Vicksburg, Miss.
- d. Environmental Laboratory. 1987. "Corps of Engineers Wetlands Delineation Manual," Technical Report Y-87-1, US Army Engineer Waterways Experiment Station, Vicksburg, Miss.

- e. Newling, C. J. 1987. "Wetland Delineation at Naval Weapons Station Concord, California," Environmental Laboratory, US Army Engineer Waterways Experiment Station, Vicksburg, Miss.
  - 2.5.2 Errata to Miscellaneous Paper EL-86-2

The following corrections are presented for the report entitled "Remedial Investigation of Contaminant Mobility at Naval Weapons Station, Concord, California" (Lee et al. 1986).

- \*page xviii; The title of Table 2-B12: Contract NBS River Sediment Analysis
- \*page 142; The word "soil" in the last sentence should be replaced by the word "solid."
- \*page 149; The horizontal axis should be: 0 1000 2000 3000 4000 5000 6000 7000 8000

- \*page 186; After the third reference on this page, insert the following: Holnigren, G. G., Meyer, M. W., Daniels, R. B., Chaney, R. L., and Kubota, J. 1987. "Cadmium, Lead, Zinc, Copper, and Nickel in Agricultural Soils of the United States," Journal of Environmental Quality (in press).
- \*page 197; Replace observation 16 with the following line: 16 BKPCW1337 0.00 0.11 C 2.91 E 0.42 B 0.43 BC 0.00 39.09 E
- \*page 210; The IDs for observations 90, 91, and 92 should be changed from K2SCW12H1, K2SCW12J1, K2SCW12K1 to ESSCW12H1, ESSCW12J1, and ESSCW12K1 respectively. The correct ID for observation 95 is K2SCW6P2.
- \*page 211; The title should be: Contract NBS River Sediment Analysis
- \*page 484 (Figure 5-3); Contractor sample IDs 29E1 and 29E2 should be 28E1 and 28E2. These corrections appear in Figure 43 (Lee et al. 1988).
- \*page 488 (Appendix 5-A); The correct IDs for sample numbers 154 and 155 are 28E2 and 28E1, respectively.
- \*pages 123 and 193 (Figure 2-60 and Table 2-A2); revised versions are presented as Figure 2.5-1 and Table 2.5-1, respectively.
- Table 2.5-2 complements information presented in Lee et al. (1986).

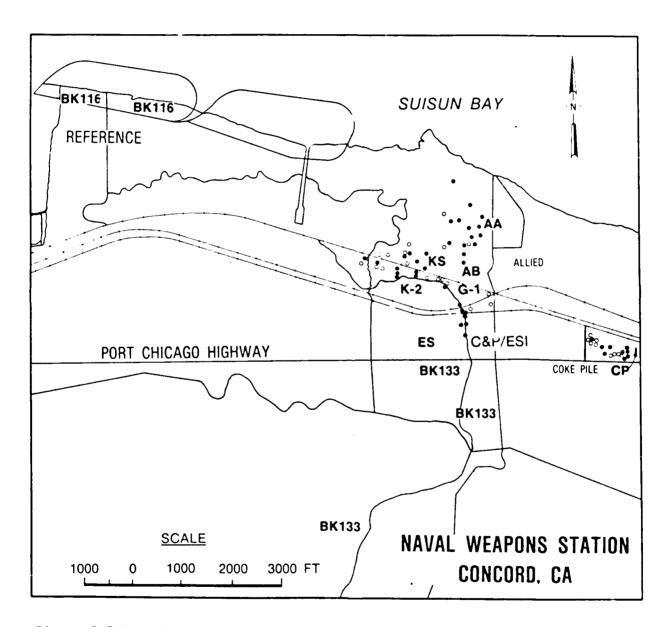


Figure 2.5-1. Distribution of soil cadmium concentrations in excess of 2.7 mg/kg. Solid circles were WES collected samples, open circles were Brown and Caldwell collected samples. (Replaces Figure 2-60, p 123, Lee et al. 1986)

Table 2.5-1\* Clam Tissue Analysis

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1.94 ABC 0.90 BCD 75.41 ABC 0.47 C 1.09 1.88 ABCDEF 0.87 CD 80.09 A 0.27 C 1.38 1.96 ABC 0.72 CD 64.28 ABCDEFGHI 0.28 C 0.52 2.26 A 0.84 CD 71.38 ABCDE 0.58 C 1.40 1.71 ABCDEFGH 0.63 D 48.02 IJ 1.01 C 1.09 2.12 A 0.72 CD 54.39 IHJGF 0.43 C 0.81 2.03 AB 0.75 CD 59.96 CDEFGHIJ 0.79 C 1.45 1.94 ABC 1.11 BCD 60.14 CDEFGHIJ 0.79 C 1.45 1.38 CDEFGH 1.12 BCD 54.01 IHJGF 0.77 C 0.74 1.15 H 0.92 BCD 61.75 CDEFGHIJ 1.31 C 1.83 1.44 BCDEFGH 0.96 BCD 72.53 ABCD 3.21 B 3.38 1.99 ABC 0.76 CD 55.01 EIHJGF 0.76 C 1.29 1.27 FGH 1.05 BCD 65.54 ABCDEFGH 5.31 A 0.26 1.17 H 1.40 B 69.22 ABCDEF 5.31 A 0.26 1.20 GH 0.63 D 51.04 IHJ 0.11 C 0.37 1.28 FGH 0.92 BCD 75.30 ABC 5.82 A 0.06	1674	1.43 BCDEFGH		55	40	0.34		45
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1.96 ABC 0.72 CD 64.28 ABCDEFGHI 0.28 C 0.52 2.26 A 0.84 CD 71.38 ABCDE 0.58 C 1.40 1.71 ABCDEFGH 0.63 D 48.02 IJ 1.01 C 1.09 2.12 A 0.72 CD 54.39 IHJGF 0.43 C 0.81 2.03 AB 0.75 CD 59.96 CDEFGHIJ 0.79 C 1.45 1.34 ABC 1.11 BCD 60.14 CDEFGHIJ 0.81 C 0.53 1.38 CDEFGH 1.12 BCD 54.01 IHJGF 0.77 C 0.74 1.15 H 0.92 BCD 61.75 CDEFGHIJ 1.31 C 1.83 1.44 BCDEFGH 0.96 BCD 72.53 ABCD 3.21 B 3.38 1.99 ABC 0.76 CD 55.01 EIHJGF 0.76 C 1.29 1.27 FGH 1.05 BCD 65.54 ABCDEFGH 5.31 A 0.26 1.17 H 1.40 B 69.22 ABCDEF 3.50 B 0.15 1.22 GH 0.63 D 51.04 IHJ 0.11 C 0.37 1.28 FGH 0.92 BCD 75.30 ABC 5.82 A 0.06	71161	1.88 ABCDEF		60	27	1.38		87
2.26 A       0.84 CD       71.38 ABCDE       0.58 C       1.40         1.71 ABCDEFGH       0.63 D       48.02 IJ       1.01 C       1.09         2.12 A       0.72 CD       54.39 IHJGF       0.43 C       0.81         2.03 AB       0.75 CD       59.96 CDEFGHIJ       0.79 C       1.45         1.34 ABC       1.11 BCD       60.14 CDEFGHIJ       0.81 C       0.53         1.38 CDEFGH       1.12 BCD       54.01 IHJGF       0.77 C       0.74         1.15 H       0.92 BCD       61.75 CDEFGHIJ       1.31 C       1.83         1.44 BCDEFGH       0.96 BCD       72.53 ABCD       3.21 B       3.38         1.99 ABC       0.76 CD       55.01 EIHJGF       0.76 C       1.29         1.27 FGH       1.05 BCD       65.54 ABCDEFGH       5.31 A       0.26         1.17 H       1.40 B       69.22 ABCDEF       5.31 A       0.26         1.22 GH       1.22 BC       66.39 ABCDEFGH       6.12 A       0.05         1.20 GH       0.63 D       51.04 IHJ       0.37         1.28 FGH       0.92 BCD       75.30 ABC       5.82 A       0.06	11162	1.96 ABC		28	28	0.52		39
1.71 ABCDEFGH 0.63 D 48.02 IJ 1.01 C 1.09 2.12 A 0.72 CD 54.39 IHJGF 0.43 C 0.81 2.03 AB 0.75 CD 59.96 CDEFGHIJ 0.79 C 1.45 1.94 ABC 1.11 BCD 60.14 CDEFGHIJ 0.81 C 0.53 1.38 CDEFGH 1.12 BCD 54.01 IHJGF 0.77 C 0.74 1.15 H 0.92 BCD 61.75 CDEFGHIJ 1.31 C 1.83 1.44 BCDEFGH 0.96 BCD 72.53 ABCD 3.21 B 3.38 1.99 ABC 0.76 CD 55.01 EIHJGF 0.76 C 1.29 1.27 FGH 1.05 BCD 65.54 ABCDEFGH 5.31 A 0.26 1.17 H 69.22 ABCDEF 3.50 B 0.15 1.22 GH 0.63 D 51.04 IHJ 0.11 C 0.37 1.28 FGH 0.92 BCD 75.30 ABC 5.82 A 0.06	11331	2.26 A		38	28	1.40		43
2.12 A 0.72 CD 54.39 IHJGF 0.43 C 0.81 2.03 AB 0.75 CD 59.96 CDEFGHIJ 0.79 C 1.45 1.94 ABC 1.11 BCD 60.14 CDEFGHIJ 0.81 C 0.53 1.38 CDEFGH 1.12 BCD 54.01 IHJGF 0.77 C 0.74 1.15 H 0.92 BCD 61.75 CDEFGHIJ 1.31 C 1.83 1.44 BCDEFGH 0.96 BCD 72.53 ABCD 3.21 B 3.38 1.99 ABC 0.76 CD 55.01 EIHJGF 0.76 C 1.29 1.27 FGH 1.05 BCD 65.54 ABCDEFGH 5.31 A 0.26 1.17 H 1.40 B 69.22 ABCDEF 5.31 A 0.26 1.22 GH 0.63 D 51.04 IHJ 0.11 C 0.37 1.28 FGH 0.92 BCD 75.30 ABC 5.82 A 0.06	11332	1.71 ABCDEFGH		02	01	1.09		47
2.03 AB 0.75 CD 59.96 CDEFCHIJ 0.79 C 1.45 1.94 ABC 1.11 BCD 60.14 CDEFCHIJ 0.81 C 0.53 1.38 CDEFCH 1.12 BCD 54.01 IHJGF 0.77 C 0.74 1.15 H 0.92 BCD 61.75 CDEFCHIJ 1.31 C 1.83 1.44 BCDEFCH 0.96 BCD 72.53 ABCD 3.21 B 3.38 1.99 ABC 0.76 CD 55.01 EIHJGF 0.76 C 1.29 1.27 FGH 1.05 BCD 65.54 ABCDEFCH 5.31 A 0.26 1.17 H 1.40 B 69.22 ABCDEFCH 5.31 A 0.26 1.22 GH 0.63 D 51.04 IHJ 0.11 C 0.37 1.20 GH 0.92 BCD 75.30 ABC 5.82 A 0.06	1333	2.12 A		39	43	0.81		32
1.94 ABC 1.11 BCD 60.14 CDEFGHIJ 0.81 C 0.53 1.38 CDEFGH 1.12 BCD 54.01 IHJGF 0.77 C 0.74 1.15 H 0.92 BCD 61.75 CDEFGHIJ 1.31 C 1.83 1.44 BCDEFGH 0.96 BCD 72.53 ABCD 3.21 B 3.38 1.99 ABC 0.76 CD 55.01 EIHJGF 0.76 C 1.29 1.27 FGH 1.05 BCD 65.54 ABCDEFGH 5.31 A 0.26 1.17 H 0.63 D 69.22 ABCDEFGH 6.12 A 0.26 1.20 GH 0.63 D 51.04 IHJ 0.11 C 0.37 1.28 FGH 0.92 BCD 75.30 ABC 5.82 A 0.06	1334	2.03 AB		96	6/	1.45		11
1.38 CDEFGH 1.12 BCD 54.01 IHJGF 0.77 C 0.74 1.15 H 0.92 BCD 61.75 CDEFGHIJ 1.31 C 1.83 1.44 BCDEFGH 0.96 BCD 72.53 ABCD 3.21 B 3.38 1.99 ABC 0.76 CD 55.01 EIHJGF 0.76 C 1.29 1.27 FGH 1.05 BCD 65.54 ABCDEFGH 5.31 A 0.26 1.17 H 1.40 B 69.22 ABCDEF 3.50 B 0.15 1.22 GH 1.22 BC 66.39 ABCDEFGH 6.12 A 0.26 1.20 GH 0.63 D 51.04 IHJ 0.11 C 0.37 1.28 FGH 0.92 BCD 75.30 ABC 5.82 A 0.06	13H1	1.94 ABC		14	81	0.53		15
1.15 H 0.92 BCD 61.75 CDEFGHIJ 1.31 C 1.83 1.44 BCDEFGH 0.96 BCD 72.53 ABCD 3.21 B 3.38 1.99 ABC 0.76 CD 55.01 EIHJGF 0.76 C 1.29 1.27 FGH 1.05 BCD 65.54 ABCDEFGH 5.31 A 0.26 1.17 H 1.40 B 69.22 ABCDEF 3.50 B 0.15 1.22 GH 6.39 ABCDEFGH 6.12 A 0.26 1.20 GH 0.63 D 51.04 IHJ 0.11 C 0.37 1.28 FGH 0.92 BCD 75.30 ABC 5.82 A 0.06	1331	1.38 CDEFGH		01	11	0.74		28
1.44 BCDEFGH 0.96 BCD 72.53 ABCD 3.21 B 3.38 1.99 ABC 0.76 CD 55.01 EIHJGF 0.76 C 1.29 1.27 FGH 1.05 BCD 65.54 ABCDEFGH 5.31 A 0.26 1.17 H 69.22 ABCDEF 3.50 B 0.15 1.22 GH 1.22 BC 66.39 ABCDEFGH 6.12 A 0.26 1.20 GH 0.63 D 51.04 IHJ 0.11 C 0.37 1.28 FGH 0.92 BCD 75.30 ABC 5.82 A 0.06	13K1	1.15 H		75	31	1.83		42
1.99 ABC 0.76 CD 55.01 EIHJGF 0.76 C 1.29 1.27 FGH 1.05 BCD 65.54 ABCDEFGH 5.31 A 0.26 1.17 H 1.40 B 69.22 ABCDEF 3.50 B 0.15 1.22 GH 1.22 BC 66.39 ABCDEFGH 6.12 A 0.26 1.20 GH 0.63 D 51.04 IHJ 0.11 C 0.37 1.28 FGH 0.92 BCD 75.30 ABC 5.82 A 0.06	13L1	1.44 BCDEFGH		53	21	3.38		78
1.27 FGH 1.05 BCD 65.54 ABCDEFGH 5.31 A 0.26 1.17 H 1.40 B 69.22 ABCDEF 3.50 B 0.15 1.22 GH 1.22 BC 66.39 ABCDEFGH 6.12 A 0.26 1.20 GH 0.63 D 51.04 IHJ 0.11 C 0.37 1.28 FGH 0.92 BCD 75.30 ABC 5.82 A 0.06	14F1	1.99 ABC		01	9/	1.29		87
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1.22 GH 1.22 BC 66.39 ABCDEFGH 6.12 A 0.26 1.20 GH 0.63 D 51.04 IHJ 0.11 C 0.37 1.28 FGH 0.92 BCD 75.30 ABC 5.82 A 0.06	131.4			22	တ္တ	0.15		9/
1.20 GH 0.63 D 51.04 IHJ 0.11 C 0.37 1.28 FGH 0.92 BCD 75.30 ABC 5.82 A 0.06	13M1	1.22 GH		39	12	0.26		97
1.28 FGH 0.92 BCD 75.30 ABC 5.82 A 0.06	4R1R	1.20 GH		04	11	0.37		69
	8P3R	1.28 FGH		30	82	90.0		24

Replaces Table 2-A2, page 193, Lee et al. 1986.

Table 2.5-2 Regression Parameters

Figure No.	Page No.	Slope	Intercept
2-72	136	0.612	0.649
2-73	137	0.338	2.924
2-74	139	0.556	19.245
2-80	146	0.455	0.958
2-81	147	0.255	1.494
2-82	148	0.306	1.520
2-83	149	0.020	4.674
2-84	150	0.697	4.554
2-85	151	0.004	143.115
2-86	153	2.524	0.577
2-87	154	98.653	9.041
2-88	155	0.927	4.568
2-89	156	4.326	4 855

# 2.5.3 Field and Laboratory Methods for Safe Handling of Contaminated Materials from the Naval Weapons Station, Concord

Because of the presence of hazardous substances in the sample areas at the Naval Weapons Station Concord, WES employees took the necessary precautions to ensure safe handling of the sampled materials. The concern was mainly to prevent any unnecessary exposure to personnel during the handling of the materials and to secure the materials and the equipment used to collect the materials in such a manner as to prevent any contamination outside the sample area.

#### 2.5.3.1 Field Sampling and Surveying

Precautions were taken in the field to prevent exposure to dusts that could be inhaled or adsorbed to the skin while WES personnel were engaged in sampling of soil materials and surveying the location of the sampled sites. Protective paper suits, boots, facial dust masks, and gloves were worn to deter contact with contaminated materials. All materials used to clean collecting equipment and discarded protective apparel were placed in an ice cooler and returned to the WES with the collected samples. These materials were placed in a sealed drum that will be shipped to an EPA-approved hazardous waste storage area. The soil samples were placed in plastic ziplock containers and sealed in ice coolers to prevent leakage and unauthorized entry during transportation.

#### 2.5.3.2 Laboratory Handling of Samples

During the preparation of the samples for laboratory analysis, precautions were taken, as in the field, to prevent exposure to personnel. Dust masks, gloves, and laboratory aprons were worn as the situation required. Contaminated lab apparel, filters, and spent soil materials were placed in a sealed drum for proper disposal. Raw and processed samples were secured under chain-of-custody procedures and stored in locked areas to prevent access by unauthorized persons.

#### 2.5.4 Clam Biomonitoring

#### 2.5.4.1 Description

The WES Ecosystem Research and Simulation Division completed a clam biomonitoring study at the NWS during the summer of 1984 (Lee et al. 1986). As a result of spring flooding in 1986, the WES initiated a second clam biomonitoring study to document possible changes in contaminant bioavailability in those areas of the NWS affected by the flood. The WES believed that substantial amounts of toxic metal-contaminated surface materials might have moved into the NWS drainage system and thereby threatened the NWS and Suisun Bay aquatic ecosystem.

The 33 sites chosen for the 1986 biomonitoring study are shown in Figure 2.5-2. Of these sites, 15 had not been monitored in 1984. These 15 were located within Parcels 571 and 572 and the property adjacent to the west of these parcels. The experimental design for the 1984 and 1986 biomonitoring studies was the same, except for the increase in the number of animals used in each cage to allow for split samples. Approximately 3,000 Corbicula fluminae were collected from the Sacramento River delta (upstream of the NWS site) and air-freighted to the WES. In addition to field testing, these clams were exposed to background chemical analysis (three replicates of 30 clams each) and Condition Indexing (Lawrence and Scott 1982). Condition Index, a good indicator of the health of the animal, was measured for 20 animals collected from the WES holding tanks the day the clams were transported to the field and on the day they were removed from the field.

The <u>Corbicula</u> were held at the WES in fiberglass tubs in aged tap water with a 3-cm layer of coarse sand. Water quality readings were made daily, and the temperature was maintained at  $15^{\circ}$  C  $\pm$   $2^{\circ}$  C. The clams were fed freshwater algae <u>Ankistrodesmus falcatus</u> and a commercial yeast mixture. The clams were slowly acclimated to a salinity level near that in the field at the NWS (2-3 ppt).

Three replicates of 25 clams each were placed at each NWS biomonitoring site for 28 days. Water quality measurements were made for each site for Days O and 28 (Table 2.5-D9). At the end of the 28-day test period, the clams were collected and placed in sealable plastic bags. They were kept cool in insulated containers during field collection and subsequent transport to the WES. At the WES they were allowed to purge their gut contents overnight in fresh aged tap water at 15° C. The clams were then prepared for metal analysis and Condition Indexing.

Tissues for metal analysis were prepared, digested and analyzed as before (Lee et al. 1986). Eleven sites were selected for Condition Index determinations (Figure 2.5-3). These samples were composed of approximately equal subsamples from each replicate at each site. Those metals (As, Cd, Pb, and Zn) demonstrating the greatest tissue uptake in the 1984 clam biomonitoring study were selected for analysis.

#### 2.5.4.2 Results and Discussion

essi persental languages indications in the second languages.

The Condition Index values for all NWS biominitoring sites (shown in Figure 2.5-4 and listed in Table 2.5-D10) were equal to or greater than the Days 0 and 28 backgound laboratory values. These data for the ratio of tissue weight to shell cavity size indicate that the clams used in the NWS biomonitoring study were actively feeding during their test period.

The water quality data from the field listed in Table 2.5-D9 showed adequate conditions for clam growth. Survival was near 100 percent for all sites except K28P3 (all three replicates lost in grass fire) and AA10S3 and AA7R1 (where one replicate sample was lost due to clam desiccation).

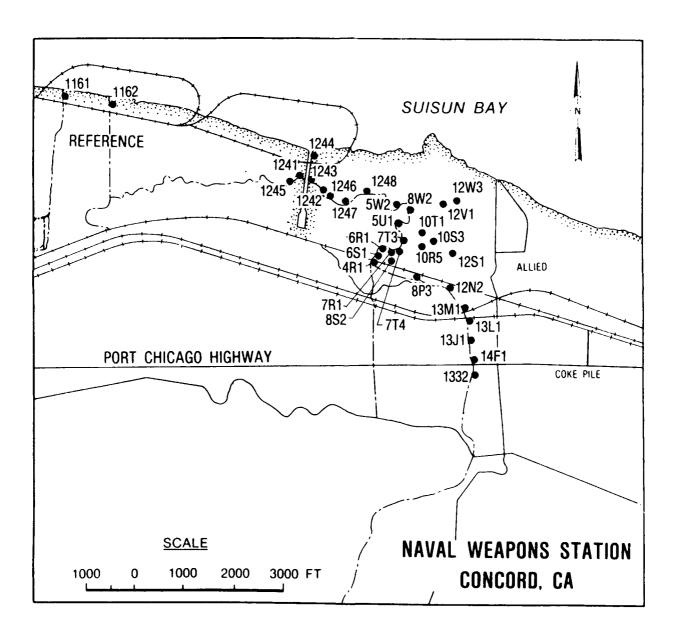


Figure 2.5-2 Clam biomonitoring locations, Naval Weapons Station, Concord, 21 May-19 June 1986

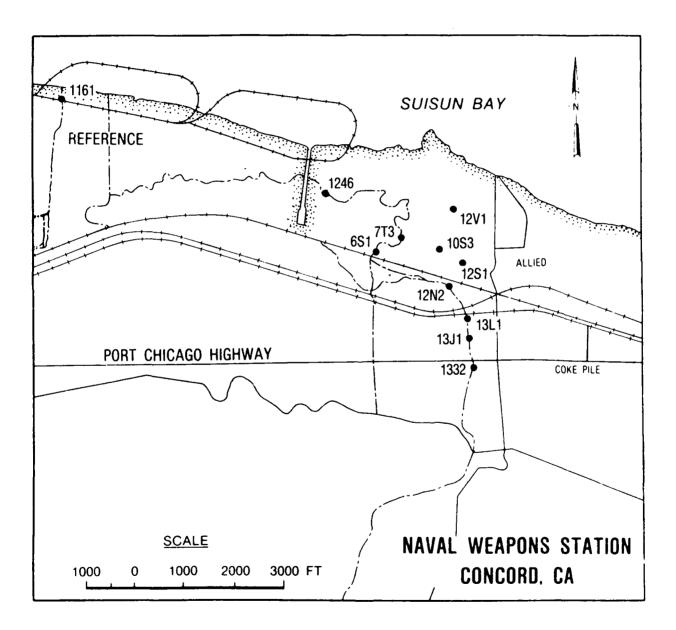


Figure 2.5-3. Condition index locations for clam biomonitoring study, Naval Weapons Station, Concord, 21 May-19 June 1986

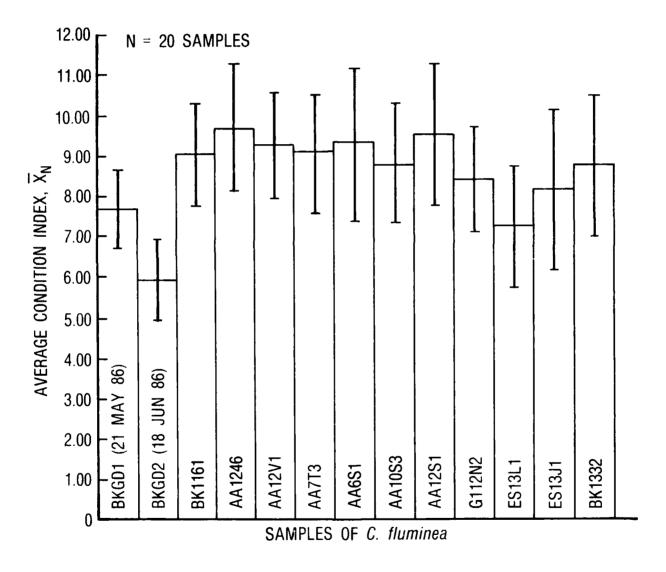


Figure 2.5-4. Average condition index values for clam biomonitoring study, Naval Weapons Station, Concord, 21 May-19 June 1986

Table 2.5-D11 represents the range of metal concentrations from the clam biomonitoring sites in 1984 and 1986 compared with literature collected field data. From these data, it is apparent that the overall metal uptake by the clams increased only slightly from 1984 to 1986. However, a large number of 1986 AA sites showed As and Zn tissue concentrations statistically above 1986 remote reference area field values as well as Cd values above those of the remote reference area in the G1 area and the AA area bordering the KS site (Table 2.5-D8).

Although the number of biomonitoring sites with tissue metal concentrations statistically above the remote reference area increased from 1984 to 1986, the metal tissue concentrations from most sites tested both years remained nearly unchanged. Thus, the increase in the number of sites containing above remote reference area tissue levels of As and Zn, and to a lesser extent Cd, was probably due to such sites not being sampled in 1984 rather than to changes in contaminant bioavailability caused by the 1986 spring flooding. The most significant clam bioaccumulation observed in 1986 was in the As tissue contents which were elevated above remote reference area in ditches that drain the AA area of Parcel 572. These data indicate some movement of As from the highly contaminated AA area, near the dike surrounding the Allied Waste Lagoon, into drainage ditches and the creek that drains the wetland.

The maximum Cd, Zn, Pb, and As tissue concentrations from this biomonitoring study did not exceed the Food and Drug Administration criteria for human consumption or the range of field-collected Corbicula from noncontaminated areas (Lee et al. 1985). In addition, the Condition Index data suggest that, during the period of 21 May - 19 June 1986, the uptake of metals by C. fluminae caused no significant physiological stress to the clams, except possibly in the ESI area. Therefore, the surface waters draining the study areas of the NWS Concord during the spring flooding of 1986 had some impact on NWS wetlands, but probably caused only a minimal increase in environmental impact on the aquatic ecosystem of Suisun Bay.

#### 2.5.5 Kiln Site Sampling

The Kiln site was subjected to an intense sampling effort. Both surface and subsurface samples were collected. These data are presented in Tables 2.5-A6, A11, A16, A26 and A31. Sample locations are shown in Figure 8.\* The analysis of variance procedure was used to analyze the data. Statistical differences were determined using the Newman-Keuls method (Winer 1971). Soil contaminated with As and Pb is confined mainly to a depth of 0 to 1 ft (Table 2.5-A32). Elevated soil Zn and Cd was observed to a depth of 3 ft in a limited number of locations. Further discussion of these results can be found in Cullinane et al. 1988.

# 2.5.6 Report of Geotechnical Fieldwork at the Kiln Site, Naval Weapons Station, Concord

A field party from the Geotechnical Laboratory, WES, installed three water sampling wells at the NWS, Concord, California for the Naval

<sup>\*</sup>Located in Lee, Cullinane, and O'Neil 1988.

Facilities Engineering Command, Western Division.

#### 2.5.6.1 Location of Wells

The wells are located around the north side of the bare ground and rubble pile in Parcel 572 known as the Kiln Site. Well separation is less than 200 ft, and the distance to the rubble pile is about 100 ft. All wells are on Navy property but within 100 ft of the railroad property line. The positions of wells are shown in Figure 2.5-5.

The locations for wells were chosen primarily to obtain the maximum sector of possible ground-water flow paths from the known source of contamination in and around the rubble pile. Private property was excluded at this preliminary stage of sampling. It was axiomatic that any discovery of contamination in the ground-water would be viewed as preliminary and would almost certainly lead to a comprehensive and sophisticated study of ground-water contamination.

By installing wells near the rubble pile, the chance of intercepting ground-water contamination from the pile was improved, as was the accessibility for the heavy drilling truck, a question of great concern before entering the site. Early visits and drilling at a site 1,600 ft to the south suggested that equipment might seriously mire down in the damp gumbo adjacent to the wetlands. A skid rig was brought to the site as a contingency but was not needed, since mobility improved with the onset of dry weather.

The site was entered from the east via the west gate from the Allied Corporation Bay Point Works. A staging area was established inside Navy property. Well 1 was located at the west to minimize disturbance of the site. The drill rig backed directly to that location and subsequently drilled wells 2 and 3 as it returned eastward to the staging area. The path followed was mostly on grass north of the bare area. Plywood sheets were used under the truck upon approaching the location for well 1 to improve mobility and to protect grass from possible rutting.

#### 2.5.6.2 Drilling

The procedure followed on all wells was the same except for depth. Wells 2 and 3 were shallower by 5 ft than well 1, since it had been found in drilling well 1 that the shallowest aquifer was fully penetrated at a depth of 15 ft. Detailed descriptions of wells 1, 2 and 3 are given in Figures 2.5-6, 2.5-7, and 2.5-8, respectively. "Aquifer" is used in a loose sense to distinguish a stratum that can transmit appreciable water as opposed to one, such as a clay-rich layer, that cannot. The scope of work for this study had generalized the possible conditions without the benefit of subsurface information. It was thought at that preliminary stage that the surface layer at the Kiln Site might be saturated, granular debris, so that the upper aquifer would be shallow and unconfined. Since the three sampling wells actually started in clay-rich soil at the surface, the anticipated conditions are irrelevant. It was still possible to follow the original intention of penetrating and sampling only the upper aquifer and bottoming in a low-permeability clay-rich layer. It was considered important that the wells not enter an aquifer below the shallowest.

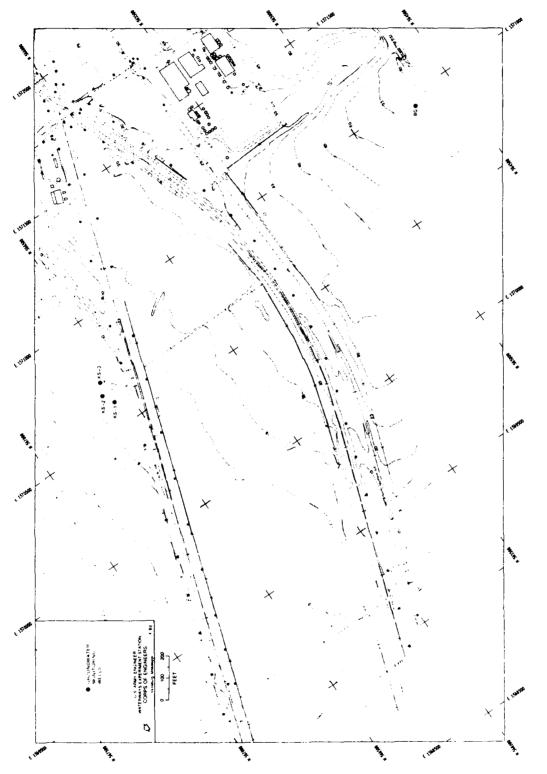


Figure 2.5-5. Location of ground-water wells, NWS Concord

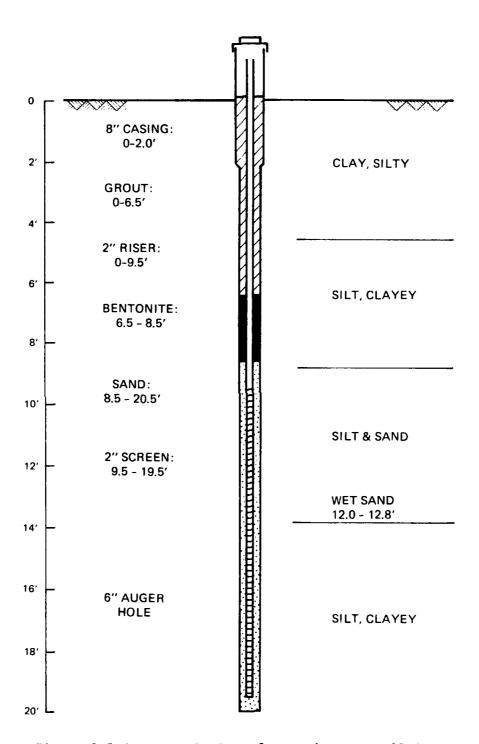


Figure 2.5-6. Description of ground-water well 1

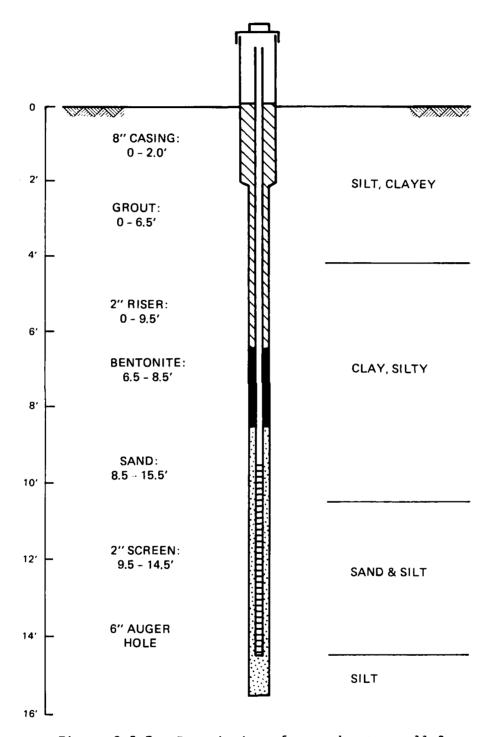


Figure 2.5-7. Description of ground-water well 2

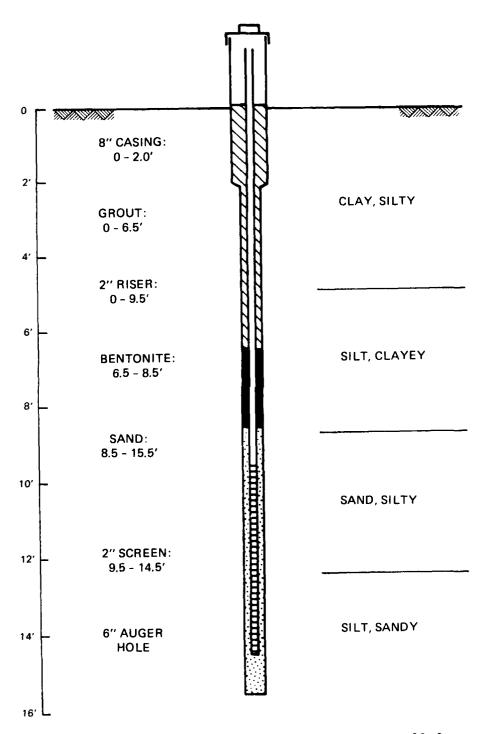


Figure 2.5-8. Description of ground-water well 3

constraint was satisfied, since even well 1 bottomed in hard, relatively dry, clayey silt.

The steps in drilling the wells followed reasonably closely to those envisioned before the work began and were as follows:

- a. Augered with 10-in. bit to ft depth.
- b. Set 8-in-diameter steel calling and grouted in place, flush with ground. This grouted casing isolates near-surface contamination.
- c. Advanced below 2-ft depth using 6-in. hollow-stem auger.
- d. Sampled soil continuously through auger stem.

#### 2.5.6.3 Well Construction

The steps in construction of the sampling well were as follows:

- a. Upon reaching final depth, added sand to 1 ft above bottom. Sand is 16 x 40 washed sand, available in bags.
- b. Placed 2-in. PVC screen and riser in hole through the stem and seated on sand bottom. Screen opening is 0.020 in.
- c. Raised auger around screen and riser while at the same time adding sand to fill space developed below. Tamped sand frequently with riser. Sections of auger were removed intermittently.
- d. Raised sand level as in step c to 1 ft above screen.
- e. Added bentonite pellets to level 2 ft above sand pack.
- f. Grouted above bentonite plug to surface.
- g. Added extension of 8-in. protective steel casing to 2 ft above ground surface and grouted around outside of joint and flanges.

The wells were developed by removing water with a gasoline-driven pump. Total volumes removed were 25, 15, and 15 gal from well 1, 2, and 3, respectively, to accomplish clarification of water from yellowish brown and translucent to a slightly cloudy but otherwise transparent condition. Flow of pump or ground-water rate ranged roughly between 0.2 and 0.4 gal/min during pumping.

#### 2.5.6.4 Health and Safety Plan

Operations at the Kiln Site were conducted according to a health and safety plan prepared especially for this investigation by technical, supervisory, and administrative personnel of the WES. The primary concerns were for health and safety of the field party. Other concerns were with safeguarding against disturbance of the site and its fauna and flora. Special attention was directed to the handling and disposal of materials

brought from depth to the surface, and all water and cuttings taken from the holes were handled and retained as hazardous material pending clearance through chemical analysis.

Soil and water collected during well installation and development were chemically analyzed to determine their hazardous nature. Results of these tests (Table 2.5-D13) indicated that the soil was not hazardous and could be disposed of in an ordinary landfill. The collected ground-water samples contained metals above drinking water quality standards and were disposed of into a sanitary sewer to protect water bodies associated with the Kiln Site on NWS Concord.

#### 2.5.6.5 Summary Observations

Salient observations deserving emphasis are as follows:

- a. All three holes appear to penetrate only natural strata from the grassy surface down. No fill or slope-wash from the rubble pile was encountered.
- b. The aquifer is at about the same position in all holes and sandwiched between relatively dry, clayey silt beds of low permeability.
- c. The aquifer is confined under a piezometric head, and water rose a few feet in all holes after first being encountered.
- d. The upper low-permeabililty layer is more than 8 ft thick. This layer presents a barrier against leakage from surficial contamination in the aquifer unless the layer has been deeply excavated.
- 2.5.7 Ground-water Sampling at the Kiln Site, Naval Weapons Station, Concord

Ground-water sampling of the monitoring wells and drums of water at the Kiln site and background well was performed on 12 May 1987. Sampling was conducted by R. Shafer (WES), P. Lacey (EMCON), and C. Schwab (Navy). A background well located about 400 feet north of Port Chicago Highway was sampled first (Lutton, Bennett, and McAneny 1987). This well was installed as a part of another study, but is located appropriately for use in this study. The 5-ft-long 2-in. PVC screen is positioned in a said aquifer, and 10 ft below the piezometric surface located at 39 ft. Prior to sampling, 10 gal of water was bailed from the well. The well water cleared up after approximately 5 gal had been removed. Five additional gallons of water was removed before sampling was conducted. Mr. Lacey concurred that a sample representative of the ground water could be obtained at this point. Prior to sampling, a distilled water field blank was obtained by placing distilled water (supplied by EMCON) in the Teflon bailer and glass sample make-up jar. The field blank was then analyzed for pH, conductivity, and temperature using EMCON's instrument. The sample was split (two subsamples for Navy, one subsample for EMCON) and preserved with nitric acid to a pH below 2.0.

The background well was then sampled using the teflon bailer and nylon rope. Approximately 0.75 gal of water was placed into the glass gallon make-up jar from the well. Measurements were taken for pH, conductivity, and temperature by Mr. Lacey. Unfiltered subsample splits were then made. The remaining sample was filtered using a 0.45-micron filter supplied by EMCON. Filtered subsample splits were made, and all subsamples were preserved with nitric acid to a pH below 2.0. The results of the field measurements are presented in Table 2.5-D12.

Monitoring well KS-1 was sampled next. Similar procedures were followed for all three wells at the Kiln site. The wells were bailed, allowed to recover, and bailed again until what was considered a representative sample could be obtained. The bailing water was placed in a drum onsite. Approximately 10, 8, and 8 gal of water were removed from KS-1, KS-2, and KS-3, respectively. The sample was then removed from the well with the Teflon bailer and placed in the glass sample make-up jar. Measurements were taken for pH, conductivity and temperature (Table 2.5-D12). Unfiltered subsamples were made and the remaining sample was filtered through a 0.45 micron filter. Filtered subsamples were then made, and all samples were preserved with nitric acid to a pH below 2.0. Duplicate split subsamples were made for the Navy for all wells except KS-3.

After sampling each well, the Teflon bailer, glass sample make-up jar, and filtering apparatus were rinsed with distilled water. Before obtaining each sample, the make-up jar and filtering apparatus were sample-rinsed with water from the monitoring well being sampled. Water levels were measured prior to bailing each well. These measurements are presented in Table 2.5-D12.

Samples were taken from two drums located onsite. These drums contained water from developing the wells at the Kiln site on 2 April 1987 (see Section 2.5.6.3) and the bailing water that was removed from wells KS-1, KS-2, and KS-3 prior to sampling on 12 May 1987. Mr. Lacey indicated that EMCON would not require a split of these samples. The samples from the two drums were not filtered. These samples were preserved with nitric acid.

The subsamples for the Navy were placed in a locked cooler. A chain-of-custody was initiated upon completion of the sampling effort. The samples were transported to WES and turned over to Mr. R. Price along with the chain-of-custody forms on 14 May 1987.

#### 2.5.8 Wetland Delineation at Naval Weapons Station, Concord

As part of an ongoing cooperative agreement between the US Naval Facilities Engineering Command, Western Division, and the WES, the Environmental Laboratory (EL) was asked to conduct a wetland delineation on Parcels 571, 572, 573, 574, 575, 576, 579D, and 581 on the NWS Concord. During the week of 3-7 November 1986, Messrs. C. J. Newling and R. Theriot traveled to the site to conduct a wetland delineation and collect the necessary field data. Various portions of this field work were observed by Drs. J. S. Wakeley and C. R. Lee and Ms. L. J. O'Neil, all of £L, who were simultaneously conducting field-work at NWS Concord, as well as

Dr. M. Josselyn of San Francisco State University and Mr. J. M. Robertson of the US Navy Office of the General Counsel.

#### 2.5.8.1 Site Description and Methods

Wetland delineations were conducted on four NWS Concord areas generally located south of Suisun Bay as outlined in Figure 2.\* site descriptions are given in Lee et al. (1986). (Figures 29, 42, and 53\* were developed from figures appearing in Lee et al. 1986). The first area (KS/AB/AA) included tidally influenced estuarine emergent marsh on Parcel 572. The second area (K-2/G-1/576) included palustrine robust emergent marsh and segments of a channelized stream on Parcels 573, 574, 575 and The third area (ES) included a channelized stream on Parcel 579D. The fourth area (CP) included palustrine robust emergent marsh on Parcel 581. Physical access was obtained to the first three areas and data were collected directly onsite. Delineation for the fourth area was based on data collected by visual observation from Port Chicago Highway and review of aerial photographs and vegetation mapping performed by Harvey and Stanley Associates, Inc. (Figure 53\* was based on a figure from the Harvey and Stanley Associates, Inc., report "Background Information for Section 7 Consultation at Concord Naval Weapons Station" dated 25 November 1986.) Methods and procedures for delineation were as described in Environmental Laboratory (1987). On the KS/AB/AA and K-2/G-1/576 areas, "comprehensive" techniques were employed. In addition, wetland and nonwetland boundary stakes were placed and later surveyed by an EL team led by Mr. J. G. Skogerboe. "Routine" techniques were used on the ES and CP areas. In mapping wetlands, delineations stopped at parcel boundaries even though wetlands extended beyond those boundaries in some cases.

#### 2.5.8.2 Results

Data collected for the KS/AB/AA area are provided in Appendix A.\*\*
When correlated with the surveyed boundary stake positions, the data supported delineating the wetland boundary along the 4.0 foot contour line and tying into lower elevation property boundaries as indicated in Figure 29.

Wetlands on the K-2/G-1/576 area were largely separated from tidal influence and occurred on a landscape with falling topography from a segment of channelized stream on the highest (east) side of the site to a broad fan of robust emergent marsh on the lowest (west) side of the site. The wetlands on the west side of the site were immediately adjacent to a tidally influenced segment of stream just off the K-2 parcel. Historically, the wetlands on this site appear to have been connected more directly to the intertidal wetlands to the north prior to construction of the railroad right-of-way that separates them. More recently, construction of the railroad right-of-way as well as stream channelization may also have had some effect on wetland plant succession by increasing freshwater influence on the site. Data collected from this area are provided in Appendix B. Plots falling at wetland boundaries were staked, and then

<sup>\*</sup>Located in Lee, Cullinane, and O'Neil 1988.

<sup>\*\*</sup>Appendixes A, B, and C are not part of this document.

surveyed for mapping purposes. The wetland boundary is indicated in Figure 42.

The wetlands on the ES area followed a channelized stream course immediately adjacent to the property boundary with the Chemical and Pigment plant (C and P/ESI area, Figure 42). The streambank slopes in most segments were very steep, with standing water or saturation to the surface in the streambed and a dense cover of vegetation dominated by Typha latifolia. Outside the distinct streambanks, wetland indicators quickly disappeared. Thus, the rather distinct boundaries of the channelized stream could be mapped as wetland for the entire course along this parcel. The mean wetland width was 11 ft. Data collected from the ES area are provided in Appendix C. The wetland boundary is indicated in Figure 42.

The wetlands on the CP area were observed from Port Chicago Highway. Based on experience gained from similar wetlands on the NWS Concord property, the plant communities observed, and the steepness of slope observed, two criteria were used to delineate the wetland boundary: the 6.0-ft contour elevation and the presence of a plant community dominated by either Typha sp. or Scirpus sp. The wetland boundary for the CP area is indicated in Figure 53.

#### 2.5.9 References

Cullinane, M. J., Jr., et al. 1988. "Feasibility Study of Contamination Remediation at Naval Weapons Station, Concord, California; Volume I: Remedial Action Alternatives," Miscellaneous Paper EL-86-3, US Army Engineer Waterways Experiment Station, Vicksburg, Miss.

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Luoma, S. N., Cascos, P. V., and Dagovicz. R. M. 1984. "Trace Metals in Suisun Bay, California: A Preliminary Report," US Geological Survey, Water-Resources Investigations Report No. 84-4170, Sacramento, Calif.

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Winer, B. J. 1971. <u>Statistical Principles in Experimental Design</u>, 2d ed., McGraw-Hill, New York.

#### 2.5.10 Sample Identification and Variable Description

#### 2.5.10.1 Tables A1-A32 Sample ID and Variable Description

Tables 2.5-A1-A31 present the soil analysis data. The samples appearing in Tables A1, A6, A11, A16, and A21 were collected in June and July 1986. Samples listed in Table A26 were collected in December 1986. The samples listed in Table A31 were collected in March 1987. Sample types SC are 0" - 6" surface samples. Sample types ST are 0" - 6" stream samples. Samples AASTW124B1D and AASTW124B2D go to a depth of 4 ft. See the variable description section below for further discussion of sample types.

#### Variable Description

#### Unit

AS, CD, CU, PB, ZN, SE

mg/kg or parts per million(ppm)

WWT AS, WWT CD.

dry weight basis

WWT CU, WWT PB, WWT ZN, WWT SE

mg/kg or parts per million(ppm)

wet weight basis

MPSOLID, SOLID

Percent solids

DI\_WT,ACT\_WT DEPTH Grams Feet

#### Example Key

ID No.: AA SCW5T2R1

Nitric acid digestion procedure used for total metal analysis

AA - Sample site area

AA: Allied A

AB: Allied B

BK: Remote reference site

CP: Coke pile site

ES: ESI

G1: G-1 Getty

K2: K-2

KS: Kiln site

SC - Sample type

SC: Soil core

ST: Soil core from a stream

GT: Surface sample gritty material

RB: Surface sample red brick YB: Surface sample yellow brick

```
W5T2R1 - Specific WES sample site location
           Label for site
     5T2
     R1, R2, R3
                 Triplicate samples
     Sample IDs in Tables A1 and A6 include D1-D4.
       D1-D4 refer to the depth of core:
               0' - 1'
          D1
               1' - \overline{2'}
          D2
               2' - 3'
          D3
          D4
               3' - 4'
       Sample IDs in Table A26 include D1-D4.
       D1-D4 refer to the depth of core:
                0" - 6"
          D1
          D2
                6" - 12"
               12" - 24"
          D3
          D4
               24" - 36"
      Sample IDs in Table A31 include D1-D6.
      D1-D6 refer to the depth of core:
               0' - 1'
          D1
          D2
               1' - 2'
          D3
               2' - 3'
          D4
               3' - 4'
          D5
               4' - 5'
          D6
               5' - 6'
       -1,S1 Split sample
```

A Sample taken June 24, 1986 B Sample taken June 25, 1986

C Resample previous contractor site

WZ_ZW	22,211111000000000000000000000000000000
WWT_PB	2812488244442241118666611119222222222222222222222222222
WWT CU	1135,500,000,000,000,000,000,000,000,000,0
WWT_CD	
WT_AS	2.50 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
ACT_WT	
DI_WT	80844441404448809988441490496888888449449649646464
MPSOLID	0822222228428428466644444444444444444444
NZ	2128 20158 201
PB	24000000000000000000000000000000000000
8	125.82.7.33.1.00.1.1.98.94.88.95.5.1.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3.
8	00000000000000000000000000000000000000
AS	21112233138421010900283118823323020202020 211128023233384201090028842626369573202020 2111203233338632303034442606060606060606060606060606060606060
OBS ID	1 AASCWSR1 2 AASCWSR2 3 AASCWSR2 5 AASCWST2R1 5 AASCWST2R1 6 AASCWST2R3 6 AASCWST2R3 6 AASCWST2R3 6 AASCWST2R3 6 AASCWST2R3 6 AASCWSTR124 1 AASTW1244 5 AASTW1244 6 AASTW1244 6 AASTW1248R1 1 AASTW1248R1 1 AASTW1248R1 2 AASTW1248B1D2 3 AASTW124B1D2 6 AASTW124B1D3 6 AASTW124B1D4R3 7 AASTW124B1D4R3 8 AASTW124B1D4R3 9 AASTW124B1D4R3 1 AASTW5R1R1 7 AASTW5R1R1 7 AASTW6R1R1
$\sim$	

	PB	0.225 0.207 0.220
Analysis	8	0000
Table 2.5-A2 Blank A	8	000.00000000000000000000000000000000000
Table 2.5	AS	0.000.0005
	Ð	BLANK-R1 BLANK-R2 BLANK-R3

OBS

ZN 0.263 0.693 0.531

Table 2.5-A3 Blank Analysis Summary

C.V.	0.000 46.398 0.000 3.275 3.813
VARIANCE	0.0000 0.0000 0.0472
MNS	0.0150 0.0036 0.0900 0.6520 1.4870
STD ERROR OF MEAN	0.0000 0.0000 0.0054 0.1254
MAXIMUM VALUE	0.0050 0.0017 0.2250 0.6930
MINIMUM VALUE	0.0050 0.0006 0.2070 0.2630
STANDARD DEVLATION	0.0000 0.0006 0.0093 0.2172
MEAN	0.0050 0.0012 0.2173 0.4957
z	നനനന
VARIABLE	88888

Table 2.5-A4 NBS River Sediment Analysis

ACT_VT	1111
DI VT	1.000
B	1598.6 1405.2 1415.2
PB	978.2 1004.1 1024.1
8	121.88 116.00 124.00
8	11.73 10.84 11.74
AS	38.81 38.25 38.35
ΙΩ	STDRS-R1 STDRS-R2 STDRS-R3
OBS	426

Table 2.5-A5 NBS River Sediment Analysis Summary

VARIABLE	z	MEAN	STANDARD DEVIATION	MINIMUM VALUE	MAXIMUM VALUE	STD ERROR OF MEAN	<b>M</b> OS	VARIANCE	C.V.
SBBBBBP PA	നനനനനന	38.470 11.436 120.626 1002.142 1473.015 1.000	0.299 0.516 4.144 23.054 108.888 0.001	38.250 10.840 116.000 978.157 1405.215 1.000 1.000	38.811 11.740 124.000 1024.135 1598.616 1.001	0.173 2.298 113.393 62.867 0.000 0.000	115.411 34.308 361.878 3006.427 4419.046 3.001	0.090 0.267 17.176 531.476 1856.694 0.000	0.778 4.514 3.436 2.300 7.332 0.058 0.058
*Stan	*Standards								
NBS	NBS River Sedime	Sediment Ana]	ent Analysis Values						
AS				0.99					
8				8.7	11.7				
8				0.06	128.0				
PB				0.989	742.0				
ĸ				1550.0	1890.0				

WT_ZN	20222 20222 202526 2025
WWT_PB	11
WAT CU	31 34 34 34 34 34 34 34 34 34 34 34 34 34
WWT_CD	02421112000LL42
WVT AS	8.1.3.0.4.3.2.4.3.2.4.2.2.2.2.2.2.2.2.2.2.2.2.2
ACT VI	011111111111111111111111111111111111111
IN_IO	8252223655555555555555555555555555555555
MPSOLID	24 W 4 W 4 W 4 W 4 W 4 W 4 W 4 W 4 W 4 W
KZ	2025288833 2025288833 2025288833 2025288833 2025288832 2025288832 2025288832 2025288832 2025288832 2025288832 2025288832 202528883 20252883 202528883 2
PB	20, 44, 20, 20, 20, 20, 20, 20, 20, 20, 20, 20
5	1200201 200201 200201 200201 200201 200201 200201 20020202 200
8	87-1488-4420-11-1880-8820-884-10-10-10-10-10-10-10-10-10-10-10-10-10-
AS	441 1
OBS ID	AASCW16U3 2 AASCW16U3 3 AASCW16U3 5 AASCW6S1 6 AASCW6S2 6 AASCW6S2 6 AASCW124B2D1 8 BASCW1332R3 10 BKSCW1332R3 11 BKSCW1332R3 12 CPSCW26F3 12 CPSCW26F3 13 CPSCW26F3 14 CPSCW26F3 15 CPSCW29E1 16 CPSCW29E1 17 CPSCW29E1 18 CPSCW29E1 18 CPSCW29E1 19 CPSCW29E1 10 CPSCW29E1 11 ESSCW13H1 11 ESSCW13K2R1 12 CPSCW13H1 13 ESSCW13K2R1 14 G1SCW13K2R1 15 G1SCW13K2R1 16 ESSCW13K2R1 16 ESSCW13K2R1 17 ESSCW13K2R1 18 ESSCW13K2R1 19 G1SCW10N4 19 G1SCW10N1 10 G1SCW1 10 G1SCW1 10 G1SCW1 10

WYT_ZN	1262.5	2/081.4 325.9	253.7	1520.9	1324.2	125.3	579.7	3951.5	409.4	223 399.8	180.6	2968.7	9084.6	147.6	526.4	842.7
WWT_PB	168.7	3610.3 239.5	82.0 79.9	249.2	295.9	46.1	193.2	629.9	56.3	33.7	53.0	227.4	1051.2	82.7	394.3	281.0 100.3
WAT_CU	25.30	441.84	33.24	56.58												157.08
WVT_CD	3.67	36.00 0.70	0.51	, , , , , , ,	2.84 0.79	0.45	2.24	7.26	1.89	0.41 9.69	0.46	16.17	23.31	0.63	1.59	.0 80.0
WWT_AS W	3.73	11.36 2.35	2.72	3.45	3.15	2.80	6.30 1.00	17.35	1.96	39.57	3.57	2.88	٠٠ 86	4.58	7.98	17.12
ACT_WT W	1.01	 	-i- 88	1.00	38	1.01	.i. 88	.0	1.04	700	1.03	1.02	88	1-	1.02	1.01
DI_WT A	1.06	1.06	1.07	1.0	1.0	1.07	1.03	1.05	1.63	7.89 40	1.58	2.17	1.93	1.07	1.15	1.06
MPSOLID I	95.21 92.05	89.64 94.28	•				•					•	•			94.85 89.31
ZZ W	1326.0	30210.9	269.1													317.4
<b>PB</b>	177.2															
5	40.33	492.90	35.26	58.63	36.50	25.59	84.27	110.82	29.05	65.09 93.09	80.03	238.37	920.04	39.04	108.02	165.60
8	3.85	40.18 0.74	0.54	3.55	7.0	0.47	2.30	7.65	2.96	9,0	0.70	34.23	44.82	0.63	1.78	6.41
AS	3.91		•				9.48	18.29	3.06	4.75	5.48	6.11	11.51	70.0	8.94	18.05 9.78
日	G1SCV12M3-1 G1SCV12M4-1	11-1 14-1	G1SCV12N4-1R2	5.7	G1SCV13M3-1 G1SCV14M2-1	2	45	K2SCV10P2	K2SCV3R3	K2SCV4P2 K2SCV403	K2SCV5P1	K2SCV5P2	K2SCV6P2	K2SCW0U1	KSSCW10R3	KSSCV10R4 KSSCV12R1

Table 2.5-A7 Blank Analysis

				•		
OBS	ID	AS	8	55	PB	Ø
-10m4s9p	NWSBLANK.R10 NWSBLANK.R4 NWSBLANK.R5 NWSBLANK.R6 NWSBLANK.R7 NWSBLANK.R7 NWSBLANK.R9	0000000	0.0001 0.00016 0.0013 0.0013 0.0013	0000000	000000000000000000000000000000000000000	0000000

Table 2.5-A8 Blank Analysis Summary

c.v.	0.000 43.033 0.000 249.259 76.932
VARIANCE	000000000000000000000000000000000000000
SUM	0.0350 0.0084 0.2100 0.1610 2.3490
STD ERROR OF MEAN	0.0000 0.0002 0.0217 0.0976
MAXIMUM VALUE	0.0050 0.0016 0.1530 0.8790
MINIMUM VALUE	0.0050 0.0001 0.0300 0.0010 0.1100
STANDARD DEVIATION	0.0000 0.00005 0.0573 0.2582
MEAN	0.0050 0.0012 0.0300 0.0230 0.3356
Z	トレトレト
VARIABLE	AS CCD CCD SN SN

Table 2.5-A9 NBS River Sediment Analysis

	A.S.			PB PB		DI W	ACT V
37	.79	11.51	116.65	686.8	1683.2	1.003	
ပိုင္တာလ	37.13 35.74	11.67 11.85	118.79	823.9 826.4	1777.6 1663.2	988	 886 898 898
33.	ম	11.82	122.76	853.7	1747.7	1.006	1.006

Table 2.5-A10 NBS River Sediment Analysis Summary

c.v.	4.308 1.245 2.136 9.917 2.865 0.164							
VARLANCE	2.410 0.021 6.549 5969.896 2403.131 0.000							
SUM	180.189 58.668 599.122 3895.417 8554.810 5.024							
STD ERROR OF MEAN	0.694 0.065 1.145 34.554 21.923 0.001							
MAXIMUM VALUE	37.787 11.854 122.763 853.728 1777.555 1.006				11.7	128.0	742.0	1890.0
MINIMUM VALUE	33.748 11.505 116.50 686.790 1663.230 1.003		S	0.99	8.7	0.06	0.989	1550.0
STANDARD DEVIATION	1.553 0.146 2.559 77.265 49.022 0.002		Analysis Values					
MEAN	36.038 11.734 119.824 779.083 1710.962 1.005		NBS River Sediment Ana					
z	ഗസസസസസ	rds	iver					
VARIABLE	AS CD CU PB ZN ZN DI WT ACT WT	*Standards	NBS R	AS	СО	CU	PB	ZN

101 106 1 106 1 106 1 106 1 107 1 10
## 1201 1201 1201 1202 1202 1203 120
### ### ### ### ### ### ### ### ### ##
11.22 12.22 13.28 14.22 14.22 15.22 16
A 0110010110110110110110110111111111111
1
MP
72 73 74 75 75 75 75 75 75 75 75 75 75
280808
QU
80.000 www.u-10.0000000000000000000000000000000000
A
AASCW10R2 AASCW10R2 AASCW10R2 AASCW10TR1 AASCW10TR1 AASCW12W1 AASCW12W1 AASCW12W2 AASCW14W1 AASCW16W2 AASC
STANDERORS AND TOUR STANDERS OF THE

	Tad	Table 2.5-ALZ	Blank	Analysis		
OBS	Ω	AS	8	8	PB	Ŋ
1264	NWSBLANK.R11A NWSBLANK.R12A NWSBLANK.R17 NWSBLANK.R18	00000	0000	0000	0000	0000

Table 2.5-A13 Blank Analysis Summary

ARIANCE C.	0.0000
SUM VARI	
EROR SI	0.0200 55 0.01100 44 0.02300
STD I	50 50 50 50 50 50 50 50 50 50 50 50 50 5
JM MAXTMUP 3 VALUE	00000
RD MINIMUN ION VALUE	0.0000
STANDARD DEVIATION	000000000000000000000000000000000000000
MEAN	0.0000000000000000000000000000000000000
Z	44444
VARIABLE	SEC SE

Table 2.5-A14 NBS Sediment Analysis 5

ACT\_WT 0.9972 0.9923 0.9990

			W S		20020000		**************************************		***************************************		
											V. POPURUK
				Table 2.5-	.5-A15 NBS		Sediment Analysis Summary	mmary			
	VARIABLE	z	MEAN	STANDARD DEVIATION	MINIMUM VALUE	MAXIMUM VALUE	STD ERROR OF MEAN	MUS	VARIANCE	c.v.	
	SSE GOS SE CONTRACTOR SE CONTR	നനനനനന	45.313 10.450 106.279 670.585 1683.852 0.996	2.619 65.1645 0.0022 0.0033 0.0033	42.593 10.289 101.660 654.752 1626.726 0.992	47.818 10.571 110.986 681.619 1755.956 0.999	1.512 0.084 2.693 88.119 0.002 0.002	135.938 31.349 318.838 2011.756 5051.555 2.989	6.861 0.021 21.751 197.740 4343.380 0.000	5.781 1.386 2.038 0.348 0.348 0.348	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~
	*Standards	lards									
	NBS	River	NBS River Sediment Analysis Values	alysis Valı	Jes						
	AS				0.99						
	8				8.7		11.7				
F	8				90.0	11.	128.0				
118	PB				686.0	77	742.0				
3	NJ.				1550.0	185	1890.0				

WT_ZN	20000000000000000000000000000000000000
WWT_PB	250 440 440 440 440 440 440 440 440 440 4
WIT CU	559473118 57947318 57
WIT CD	01040000000000000011404000000011440040004011011
WWT_AS	8082221899 085175 8082521899 08575 8082521896 8085256 808526 8085256 808526 8085256 8
ACT_VT	
D DI WT	41111121111211111111111111111111111111
MPSOLID	070703088889202088888864744449086444444602244444602244444602244444602244444602244444460224444446022444444602444444602444444460244444444
ĸ	215.25.55.55.55.55.55.55.55.55.55.55.55.55
PB	15. 12. 12. 12. 12. 12. 12. 12. 12. 12. 12
몽	1102448889450114488695144887514445670748868751448876114484876114487676144487676144487676144487676144487676144487676744887676744887676744887676744487676744887676744444444
8	08-140000000000008-104000-001-0040000000000
AS	5004441000 8000 8000 8000 8000 8000 8000
£	AASCV10S1 AASCV11R1R1 AASCV11R1R2 AASCV12R3 AASCV12R1 AASCV12R1 AASCV12R1 AASCV12R1 AASCV16V3R1 AASCV16V3R1 AASCV16V3R1 AASCV16V3R1 CPSCV29E2R1 CPSCV29E2R1 CPSCV29E3R3 CPSCV29F3R2 CPSCV29F3R3 CPSCV29F3R3 CPSCV29F3R3 CPSCV29F3R3 CPSCV29F3R3 CPSCV29F3R3 CPSCV29F3R3 CPSCV30F4 CPSCV30F4 CPSCV30F4 CPSCV30F4 CPSCV30F4 CPSCV13V3 CPSCV13V3 CPSCV13V6 CISCV110N3 CISCV110N3 CISCV12M6 CISCV12M6 CISCV12M6 CISCV12M6 CISCV12M6 CISCV13M4 CISCV13M4 CISCV13M4 CISCV13M4
OBS	44444444444444444444444444444444444444
_	A CONTRACT OF THE PROPERTY OF A CANADA CANAD

WT ZN	44,4699 44,46194 45,5134 46,5135 46,513 4	3/0.0
WWT_PB	11170 9976 4184 14188 1225 1225 1373 1373 1373 1373 1373 1373 1373 137	
WITCH	1255.59 1355.55 135	
WITCD	27.72 27.72 27.72 27.72 27.73 27.73 27.73 27.73	3
r wyt as	4444082400444044244846 28609644888668481818	
T ACT_VT	4444440044440440044 4444440044440440044	10.1
TV_IG GI		
MPSOLID	28888888888888888888888888888888888888	, X
K	20759.15 5079.23 5079.23 5033.77 5033.77 5017.33 5017.	7.07
PB	122 22 22 22 22 22 22 22 22 22 22 22 22	
CG	65.50 110.61 114.81 107.63 1153.37 134.82 140.66 140.66 140.66 168.89 168.89 168.89 103.33	74.7
8	380.7.5.000.3.36.00.00.3.36.00.00.3.36.00.30.00.0	
AS	444440620111 500802020111 5008020202011 50080202020 500802020 500802020 50080 5008020 50080 50	7
QI	G1SCV13M5R3 G1SCV14L2R1 G1SCV14L2R3 G1SCV14L2R3 G1SCV14K13 G1SCV14K13 G1SCV14K13 G1SCV3P3 K2SCV3P3 K2SCV4P1 K2SCV4P1 K2SCV4P1 K2SCV4P1 K2SCV4P1 K2SCV4P1 K2SCV4P1 K2SCV4P1 K2SCV6P1 K2SCV6P1	X

Table 2.5-A17 Blank Analysis

	labi	labie 2.3-Ai/ blank		Analysis		
BS	Ð	AS	8	8	PB	NZ.
1264	NVSBLANK.R11B NVSBLANK.R12B NVSBLANK.R13 NVSBLANK.R14	00000	000000000000000000000000000000000000000	00000	00000	0000
<b>ر</b> م	NWSBLANK.R15	200		000	35	0.29

Table 2.5-A19 NBS Sediment Analysis

	ACT_VT	1.0089 0.9989 1.0083 1.0050
	DI_VT	1.0089 0.9989 1.0083 0.9937 1.0050
	ĸ	1599.96 1651.02 1506.69 1609.34 1556.42
	PB	505.3 1020.9 488.8 533.2 557.0
	8	100.11 118.63 97.69 106.17 103.98
	8	10.18 11.24 9.89 11.80 9.78
l	AS	36.97 38.29 37.89 40.51 45.12
	Ωī	NVSSTDRS.RS10B NVSSTDRS.RS11 NVSSTDRS.RS12 NVSSTDRS.RS13 NVSSTDRS.RS14

Table 2.5-A20 NBS Sediment Analysis Summary

C.V.	8.226 8.447 7.730 36.241 3.474 0.650							
VARIANCE	10.695 0.798 0.798 66.267 50656.563 3030.630 0.000							
SUM	198.778 52.890 526.578 3105.193 7923.428 5.015							
STD ERKOR OF MEAN	1.463 0.463 3.641 100.654 24.620 0.003							
MAXIMUM VALUE	45.124 11.799 118.630 1020.933 1651.016 1.009				11.7	128.0	742.0	1890.0
MINIMUM VALUE	36.971 9.776 97.689 488.753 1506.694 0.994		es	0.99	8.7	0.06	0.989	1550.0
STANDARD DEVIATION	3.270 0.894 8.140 225.070 55.051 0.007		NBS River Sediment Analysis Values					
MEAN	39.756 10.578 105.316 621.039 1584.686 1.003		Sediment Ar					
z	ഹസസസസസ	*Standards	River					
VARIABLE	AS CD CU CD ZN ZN DI VT ACT VT	*Sta	NBS 1	AS	8	CG	PB	NZ

	WWT_SE	22.22.00000904.11.1.1.0.4.0.00000000000000000
d July 1986	SE	22 22 22 22 23 24 25 25 25 25 25 25 25 25 25 25 25 25 25
is (June and	ACT_WT	000000000000000000000000000000000000000
Soil Analysis	DI_WT	11111111111111111111111111111111111111
Table 2.5-A21 S	MPSOLID	8999989899999999999988822434444 6744644196666666666666666666666666666666
	ID	CPSCV26F1 CPSCV26F1 CPSCV26F2 CPSCV26G3 CPSCV26G4 CPSCV26G5 CPSCV26G5 CPSCV27E1 CPSCV27E1 CPSCV29E10 CPSCV29E11R3 CPSCV29E1R2 CPSCV29E1R2 CPSCV29E2R1 CPSCV29E3 CPSCV29E3 CPSCV29E3 CPSCV29E3 CPSCV29E3R2 CPSCV29E3R2 CPSCV29E3R1 CPSCV29E3R1 CPSCV29E3R1 CPSCV29E3R1 CPSCV29E3R1 CPSCV29E3R1 CPSCV29E3R1 CPSCV29E3R1 CPSCV29E3R3 CPSCV29E3R1 CPSCV30F1 CPSCV30F1 CPSCV30F1 CPSCV30F4 CP
	OBS	10000000000000000000000000000000000000

Table 2.5-A22 Blank Analysis

	<b>—</b> с	NWSDLAINK, KLIA	
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Table 2.5-A23 Blank Analysis Summary

STATES CONSISSION TO SOUTH PASSOCIAL DESCRIPTION OF THE SOUTH SOUT

ر. م	Ċ
VARIANCE	C
MUS	0,080
STD ERROR OF MEAN	C
MAXIMUM VALUE	0.0200
MINIMUM VALUE	0.0200
STANDARD DEVIATION	0
MEAN	0.0200
Z	7
VARIABLE	SE

	Table 2.5-A24 NBS Sediment Analysis	Sediment	Analysis	
OBS	ID	IV_IG	ACT_WT	S
1785	NWSSTDRS-RS4 NWSSTDRS.RS10A NWSSTDRS.RS12 NUSSTDRS PS15	1.003 0.997 1.008	1.003 0.997 1.008	0000

Table 2.5-A25 NBS Sediment Analysis Summary

c.v.	0.695	
VARIANCE	0000	
SUM	4.001 4.001 0.605	
STD ERROF OF MEAN	0.003 0.003 0.151	
MAXIMUM VALUE	1.008 1.008 0.605	
MINIMUM VALUE	0.992 0.992 0.000	
STANDARD DEVIATION	0.007	
MEAN	1.000.151	
z	444	S
VARIABLE	DI VT ACT VT SE _	*Standards

This value is not certified because it is not based on the results of either a reference method or two or more independent methods. Note:

Se

NBS Sediment Analysis Value

WYT ZN	111719673888862113000644175170 11177166733482775113000698110888671171000678477517000678471700067871700006787170000678717000067871700006787170000678717000067871700006770000677000067700000067700000000
WVT_PB	11221123 882 211211221333333333333333333
WATCU	22 22 22 22 22 22 22 22 22 22 22 22 22
WWT_CD	
WWT_AS	22
MPSOLID	2444944488888882888888888882282222222222
ZN	223378 223378 223378 223378 223378 223378 223378 223378 223378 223378 223378 223378 223378 223378 233378
PB	110040448000000000000000000000000000000
23	828894008421424 22 22 22 22 22 22 22 22 22 22 22 22
8	worto40nwrosi44nimo4mo600nmmno24rmo1044ninumum4no440 eero64nimona40mrocommina6mina6mina6mina6mina6mina6mina6mina
AS	01 0201 01 0202
ID	AASCVI 6U5 AASCVI 6U6 AASCVI 6U6 AASCVI 6U6 AASCVI 6U6 ABSCVI 502 ABSCVI 552 ABSCVI 553 ABSCVI 553 ABSCVI 553 ABSCVI 553 ASCVI 553 ASCVI 001D2R1 KSSCVI 001D2R2 KSSCVI 001D2R3 KSSCVI 001D2R3 KSSCVI 002D2R1 KSSCVI 002D3 KSSCVI 002D4 KSSCVI 002D4 KSSCVI 002D4 KSSCVI 002D4 KSSCVI 002D1 KSSCVI 002D1 KSSCVI 002D1 KSSCVI 002D1 KSSCVI 101D2 KSSCVI 101D2 KSSCVI 101D2 KSSCVI 102D1
0 <b>BS</b>	44444444444444444444444444444444444444

WT_ZN	1,000 1,000	11200 10004 10	۲,
WWT_PB		5 5 5 4 4 4 5 6 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	_
WWT_CU	,	28712111142 287212111142 287212211114 287212211114 207212112114 207212114 207212114 20721214 207214 207214 20721214 207214 20721214 20721214 20721214 20721214 20721214 20721214 20721214 20721214 20721214 20721214 20721214 20721214 207214 20721214 20721214 20721214 20721214 20721214 20721214 20721214 20721214 20721214 20721214 20721214 20721214 207214 20721214 20721214 20721214 20721214 20721214 20721214 20721214 20721214 20721214 20721214 20721214 20721214 20721	
WWT_CD		######################################	
WWT_AS	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	201184848411 500400000420000000000000000000000000000	
MPSOLID	277 277 277 278 277 277 277 277 277 277	0179024888888888888888888888888888888888888	
ZN	H00HH00H0000H	11001 7004 7004 7004 7004 7004 7004 7004	<b>.</b>
PB	2014600040004000000000000000000000000000	, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	•
n D	000000000000000000000000000000000000000	041 041 051 052 052 053 054 055 055 055 055 055 055 055	
8	400000000000000000000000000000000000000	28841 887-8444441000448641410000000000000000000000	•
AS	\$1.00044m1.01.040m0	80 4 6 4 6 4 6 4 6 4 6 6 6 6 6 6 6 6 6 6	•
ID	SSSCW1102 SSSCW1103 SSSCW1103 SSSCW1103 SSSCW11103 SSSCW111R5 SSSCW111R5 SSSCW111R5 SSSCW111R5 SSSCW111R5	KSSCW11R6D1 KSSCW11R6D2 KSSCW11R6D3 KSSCW11R6D3 KSSCW11R7D2 KSSCW11R7D2 KSSCW11R8D1 KSSCW11R8D2 KSSCW11R9D1 KSSCW11R9D2R3 KSSCW11R9D2R3 KSSCW11R9D2R3 KSSCW11R9D2R3 KSSCW11R9D3R3 KSSCW12Q1D3 KSSCW12Q1D3 KSSCW12Q1D3 KSSCW12Q1D4 KSSCW12Q1D4 KSSCW12Q1D4 KSSCW12Q1D4 KSSCW12R4D3R3 KSSCW12R4D3R3 KSSCW12R4D3R3 KSSCW12R4D3R3 KSSCW12R4D3R3 KSSCW12R4D3R3 KSSCW12R4D3R3	SSCW12K4

	WY ZN	22232 22232 245033	283 1015 391 225 246 548 694	1186 1345 1345 1904 200 230		785 746 746 1357 26,6	22 3710 2079 1210 1339 1675 625	70 406 269 6299 964
	WWT_PB			٩	~4m0,4ma	0001 0001 0001 0001 0001 0001 0001 000		wr.40wn
	WWT_CU	13.8 123.3 6.5 21.4 21.4	02843. 05843.	105 582 587 505 505 505 505 505 505 505 505 505 50	222.6 222.6 222.6 25.6 25.6	2222 2333 2122 2122 242 242 242 242 242 242 242 2	200.75 173.27 173.27 173.27 173.27 173.27	20.4 25.3 31.5 14.0 14.0
	WVT_CD					2000000		
	WWT_AS		14.00m.0m0			,000,044,0 ,000,000,000,000,000,000,000,		
)	MPSOLID	90. 70. 70. 70.	922.5	98889	8002088	00000000000000000000000000000000000000	\$0.440 0.00	70000XX
	NZ.	49 22 40 311 117	$a_{\mathcal{O}}$	11303 1472 12883 25283 25883 25083 25083	1 - 0 1 7 0 001 - 0	28889 2888 3988 3988 3988 3988 3988 3988	26. 3823 3823 2228 2648 2273 948	
) 1	PB					1,22 1,22 1,23 1,03 1,03 1,03 1,03 1,03 1,03 1,03 1,0	V	400000
201	CG	mown voc.	222. 222. 225. 236.	, , , , , , ,	7.004.00	20.02 20.03 20.03 20.03	7.182347.5	
	8				00000000000000000000000000000000000000		200.2 1.2 1.2 1.2 1.2 1.2	2000034 20100034
	AS		,000,000,00c	· · · · · · ·		477 5 5 6 7 7 7 7 7 7 7 7 7 7 7 7		
	ΙD	SSCV12R5D SSCV12R5D SSCV12R5D SSCV12R5D SSCV12R6D SSCV12R6D	SSCV12R6D3 SSCV12R6D4 SSCV1301D1 SSCV1301D3 SSCV1301D4 SSCV1301D4 SSCV1301D4	SSCV13R1D SSCV13R1D SSCV13R1D SSCV13R1D SSCV13R1D SSCV13R1D	SSCVIBRED SSCVIBRED SSCVIBRED SSCVIBRED SSCVIBRED SSCVIBRED SSCVIBRED	KSSCW1, K3D4 KSSCW13R4D1 KSSCW13R4D2 KSSCW13R4D4 KSSCW13R5D1 KSSCW13R5D1 KSSCW13R5D2	SSC488301 SSC488301 SSC488301 SSC488303 SSC488303 SSC488304 SSC488401	SSCURE SS
	)BS	200 001 001 001	200000	112777	122 122 123 123 123	100 100 100 100 100 100 100 100 100 100	32654325	1730 1740 1747 1743 1743

	WT ZN	985 1708 2159 2539 10820 10435 11378 867 753
	WWT_PB	38875793 2.23375756 2.23375756 2.23875756 2.298100088
	WVT_CU	2228 309.99 1001.100 116.39 116.99 116.99
	_	00700000000000000000000000000000000000
		11000000000000000000000000000000000000
Concluded)	MPSOLID	7,000000000000000000000000000000000000
^	ZZ	1378 3098 3098 119998 117748 12773 1368 1090
Table 2.5-AZ	PB	2,44,000 10,500 10,500 10,500 10,500 10,000
	B	262.5 262.5 262.5 262.5 262.5 261.5 261.5 33.9
	C	80000840000000000000000000000000000000
	AS	44.70.00.00.00.00.00.00.00.00.00.00.00.00.
	ID	KSSCW902D3 KSSCW902D4R1 KSSCW902D4R2 KSSCW903D1 KSSCW903D2 KSSCW903D4 KSSCW9R1D1 KSSCW9R1D2 KSSCW9R1D2 KSSCW9R1D3
	S	5/2/280/0H28/410/0

PB	005
	00
5 000000000000000000000000000000000000	0.0
cD 0.005 0.0	0.007
Table 2.5-A27 Blank Analysis  AS CD  0.005 0.003  0.005 0.005  0.005 0.005  0.005 0.008  0.005 0.008  0.005 0.006  0.005 0.010  0.005 0.010  0.005 0.004  0.005 0.005  0.005 0.004  0.005 0.005  0.005 0.005  0.005 0.005  0.005 0.005  0.005 0.005  0.005 0.006	0.006
ID BLANKR1 BLANKR10 BLANKR11 BLANKR12 BLANKR14 BLANKR15 BLANKR15 BLANKR16 BLANKR16 BLANKR2 BLANKR3 BLANKR3 BLANKR3 BLANKR5 BLANKR5 BLANKR5 BLANKR5 BLANKR5	BLANKR8 BI ANKR9
0BS 110 111 112 113 113 114	16 17

Table 2.5-A28 Blank Analysis Summary

c.v.	7.351 58.011 2.411 33.640 35.774
VARIANCE	0.0000014 0.00001685 0.0000053 0.0000026
SUM	0.0870 0.1203 0.5130 0.0260 0.6870
STD ERROR OF MEAN	0.00009125 0.00099563 0.00017647 0.00012478 0.00350636
MAXIMUM VALUE	0.0065 0.0152 0.0330 0.0820 0.0840
MINIMUM VALUE	0.00000 0.0010 0.0010 0.0010
STANDARD DEVIATION	0.00037622 0.00410511 0.00072761 0.00051450 0.01445709
MEAN	0.00511765 0.00707647 0.03017647 0.00152941 0.04041176
Z	71 71 71 71
VARIABLE	SS CCD SN

					•	
BS	ID	AS	8	CG	PB	.,
765543210987654321	RIVERSEDIMENTRIORIVERSEDIMENTRIORIVERSEDIMENTRIIRIS RIVERSEDIMENTRIIRIVERSEDIMENTRIIRIVERSEDIMENTRIIRIVERSEDIMENTRIIRIVERSEDIMENTRIIVERSEDIMENTRIIVERSEDIMENTRIIVERSEDIMENTRIIVERSEDIMENTRIIVERSEDIMENTRIIVERSEDIMENTRIIVERSEDIMENTRIIVERSEDIMENTRIIVERSEDIMENTRIIRI	7444000044444444 70001000000000000000000000000000000000	99112110011111 14822287224499711	00000000000000000000000000000000000000	2000 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	

Table 2.5-A30 NBS River Sediment Analysis Summary

gerata **ecococo desta segetal e locata esta kastados esta por esta** 8. 8.

c.v.	11.728 9.039 4.006 24.683 5.448							
VARIANCE	33.66 1 0.95 0.95 14.68 32826.52 7650.37							
SUM	840.95 183.48 1625.85 2478.70							
STD ERROR OF MEAN	1.407 0.237 0.929 43.943 21.214							
MAXIMUM VALUE	60.74 12.20 100.99 1079.92 1822.98				11.7	128.0	742.0	1890.0
MINIMUM VALUE	41.74 9.15 89.49 467.42 1442.98			0.99	8.7	0.06	0.989	1550.0
STANDARD DEVIATION	5.801 0.976 3.831 181.181 87.466		NBS River Sediment Analysis Values					
MEAN	49.47 10.79 95.64 734.04 1605.33		.ment Ana]					
z	1177	ι,	Sedi					
VARIABLE	AS CU CU ZNB ZNB	*Standards	NBS River	AS	G	CU	PB	ZN

١.		

SOLID	89889778888877777777777777777777777777
K	22 29 8
SE	
PB	222224 2222238223332222222338222222223332222222
55	111
8	7.1.2.2.1.1.0.2.1.1.0.1.0.1.0.1.0.1.0.2.0.0.0.0
AS	15.2020 2.2033 2.2034 2
WWT ZN	7, 17, 2, 2, 2, 2, 2, 2, 2, 2, 2, 2, 2, 2, 2,
WWT_SE	00000000000000000000000000000000000000
WWT PB	00000000000000000000000000000000000000
WWT CU	282224 28224 28224 28224 28224 28224 28224 28224 28224 28224 28224 28224 28224 28224 28224 2822
WWT CD	
WWT AS	22222222222222222222222222222222222222
OBS DEPTH ID	10

Table 2.5-A31 Soil Analysis (March 1987)

	SOLID	004 81.7 229 77.7 297 77.7 202 77.7 205 77.7 205 77.7 207 77.7 207 88.0 207 77.7 207 81.0 45 99.0
	NZ.	2563 88623 7687 7687 7687 77687 77687 77687 777 77
	SE	20000000000000000000000000000000000000
	PB	134.64 255.74 19.64 177.20 256.13 256.13 13.58 211.52 211.52
	8	477 553.36 553.38 288.51 3056.37 522.38 53.78 53.78 53.78 53.78
	8	11.6551 8522 11.1.1.2.2.88 11.1.2.2.6.88 11.1.2.2.6.88
	AS	133.853 144.10 44.10 28.23 28.75 28.75 370.66 37.166 32.10 32.10 307.85
3	WT_ZN	6460 66460 6670 6670 6670 6670 6670 6670
	WWT_SE	20000000000000000000000000000000000000
	WWT_PB	2011 2012 2014 2014 2014 2014 2014 2014
	WAT CU	4390 4300 7220 7220 7300 7300 7300 7300 7300 7
	WWT_CD	27.7.10 27.7.00 27
	WWT AS	539 104.00 104.00 288.336.00 26.2246.00 36.226.00 36.206
	QI	KSSCW1108D1S1 KSSCW1108D2S1 KSSCW1108D4S1 KSSCW1108D4S1 KSSCW1108D6S1 KSSCW1109D1S1 KSSCW1109D2S1 KSSCW1109D5S1 KSSCW1109D5S1 KSSCW1109D6S1 KSSCW1109D6S1 KSSCW1109D6S1
	S DEPTH	012w42012w420 12w42012w420

Table 2.5-A32 Mean Soil Analysis

* Depth	As	Cd	Cu	Pb	Se	Zn
0-1	429.7A	3.2BC	257.2AB	137.0A	1.03A	277.5BC
1-2	127.5B	5.0AB	387.0A	26.0B	1.27A	459.4AB
2-3	47.4B	6.9A	173.6BC	18.3B	1.41A	658.6A
3-4	51.5B	3.5BC	136.0BC	16.5B	1.30A	264.8BC
4-5	46.8B	1.8CD	18.6CD	16.8B	1.11A	106.4CD
5-6	35.9B	1.4CD	16.2CD	16.0B	0.97A	70.3CD

Values are mg/kg dry wt.

<sup>\*</sup> Depth in feet.

# 2.5.10.2 Tables B1-B7 Sample ID and Variable Description

Tables 2.5-B1-B7 present the wet extraction analysis data. The samples that appear in Tables B1 and B4 were collected in June and July 1986. Samples listed in Table B5 were collected in December 1986.

## Variable Description

Unit

WWT\_AS,WWT\_CD, WWT\_CU,WWT\_PB,WWT\_ZN mg/kg or parts per million(ppm)
wet weight basis

W EXT

Grams

#### Example Key

ID No.: WT AA SCW5T2R1

WT - Wet extraction procedure of California State Department of Health Sciences used for analysis

AA - Sample site area

AA: Allied A

AB: Allied B

CP: Coke pile site

ES: ESI

G1: G-1 Getty

K2: K-2

KS: Kiln site

SC - Sample type

SC: Soil core

W5T2R1 - Specific WES sample site location

5T2 Label for site

R1, R2, R3 Triplicate samples

Samples IDs in Table B5 included D1-D4.

D1-D4 refer to the depth of core:

D1 0" - 6"

D2 6" - 12"

D3 12" - 24"

D4 24" - 36"

- A Sample taken June 24, 1986
- B Sample taken June 25, 1986
- C Resample previous contractor site

Table 2.5-B1 Wet Extraction (June and July 1986)

- 1	25.07 25.01 25.00 25.10	25.05 24.99 25.11	25.25 25.05 25.05	1222 1255 1256 1256 1256 1256 1256 1256	25.55 25.03 28.03 28.03	255.02 25.04 25.04	25.02	24.98 24.97	25.03 25.03	327 329 389 389	25.02 25.03 0.04	25.05 25.00 25.00	25.09 24.91	25.05 25.01	25.10 24.98	24.91 24.97 24.97	24.99 24.99	25.00 25.00 25.00
- t	199.87 5.45 2.91 3.48	6.00 6.00	2010	4.00	imod	مفد	أمرانا	જે છે		• •	• •					• •		32.07 10.17
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	10.185 0.222 1.285 3.235	1.185 2.415 14.985	8.175 10.585	26.585 1.265 2055	0.726	0.0/3 0.145 905	1.045 16.585	0.963 9053 9053	8.425 6.515 5.515		2.945 005 005	3.395 2.255	1.735	0.875 0.232	2.215 2.665	4.725 4.295 4.155	0.318 0.318 0.55	9.675 0.708
- 1	0.7590 0.0006 0.0006	0.0078 0.0136 0.1890	0000	0.002	0000	0.00/3 0.0196 0.154	0.0032	0.0091 0.0986	0.0181	0.0450	0.0498	0.0032	0.0374	000	0.0035 0.0014	0.0042	0000	0.0960
								യ്ഗ്		·••	•	4.0		200	ښز			
חד	WTAASCW10R2 WTAASCW10S1 WTAASCW10S2	WTAASCW1OT1R2 WTAASCW1OT1R3 WTAASCW11R1R1	WTAASCWIIRIRZ WTAASCWIIRIR3 WTAASCWIIRIR3	WIAASCW1251 WIAASCW1271 WIAASCW1271	WTAASCW12W2 WTAASCW14W1	WTAASCW14XZ WTAASCW16U1 UTAASCW16I12	VTAASCV16U3 VTAASCV16U4	WTAASCW16V1 WTAASCW16V2	WTAASCW16V4 WTAASCW16V4	WIAASCW16WI WIAASCW16W2R1	WIAASCW16WZRZ WTAASCW16WZR3 UTAASCW16W3R1	WTAASCW16W3R2 WTAASCW16W3R3	WTAASCW16W4 WTAASCW16X1	WTAASCW16X3	WTAASCW16X5	WIAASCWI6X6KI WIAASCWI6X6R2		WTABSCW14R1 WTABSCW14R1 WTABSCW14S1
	ID WWI AS WWI CD WWI ED WWI EAR	NR2 1.355 0.7590 10.185 3.229 199.87 25. NS1 4.205 0.0006 0.222 0.117 5.45 25. NS2 3.945 0.0000 1.285 0.769 2.91 25. NTIR1 8.855 0.0034 3.235 2.289 3.48 25.	RZ 1.355 0.7590 10.185 3.229 199.87 25.052 0.0006 0.222 0.769 2.91 25.052 0.0000 1.285 0.769 2.91 25.0117 9.955 0.0078 1.185 1.979 3.35 25.01183 4.085 0.0078 1.185 1.979 3.35 25.01183 1.875 0.186 1.985 0.588 3.0099 7.16 24.187 1.885 0.0078 1.485 0.588 3.0078 1.285 0.588 3.0078 1.285 0.588 3.0078 1.285 0.588 3.0078 1.285 0.588 3.0078 1.285 0.588 3.0078 1.285 0.588 3.0078 0.588 3.0	NR.2 1.355 0.7590 10.185 3.229 199.87 25. 0.7590 10.222 0.117 5.45 25. 0.222 0.0006 0.222 0.117 5.45 25. 0.117 5.45 25. 0.0004 1.285 0.769 2.91 25. 0.0034 3.235 2.289 3.48 25. 0.0078 1.185 1.979 3.35 2.289 3.35 25. 0.0078 1.185 1.979 3.35 25. 0.0034 1.185 0.588 30.97 25. 0.0030 8.175 0.319 22.97 25. 0.004 1.255 0.0690 8.275 0.004 1.77 25. 0.004	National Property   Nati	1.355	NR.2 1.355 0.7590 10.185 3.229 199.87 25.77 289 3.348 3.0000 10.0000 1.285 0.769 3.348 2.55 0.0000 1.285 0.0000 1.285 0.0000 1.285 0.0000 1.285 0.0000 1.285 0.0000 1.285 0.0000 1.285 0.0000 1.285 0.0000 1.285 0.0000 1.285 0.0000 1.285 0.0000 1.285 0.0000 1.285 0.0000 1.288 30.97 22	1.355	MILES 1.355 0.0006 0.222 0.117 0.222 0.117 0.0009 0.1285 0.0009 0.222 0.117 0.0009 0.117 0.0009 0.1185 0.0009 0.117 0.0009 0.1185 0.0009 0.1185 0.0009 0.1185 0.0009 0.1185 0.0009 0.1185 0.0009 0.1185 0.0009 0.1185 0.0009 0.1185 0.0009 0.1185 0.0009 0.1185 0.0009 0.1185 0.0009 0.1185 0.0009 0.1185 0.0009 0.1185 0.0009 0.1185 0.0009 0.1185 0.0009 0.1195 0.0009 0.0009 0.1195 0.0009 0.000	RESTRICT TO THE PROPERTY OF TH	1.355   0.7590   0.117   0.7590   0.0000   0.117   0.0000   0.117   0.0000   0.117   0.0000   0.117   0.0000   0.117   0.0000   0.0000   0.117   0.0000   0.0000   0.117   0.00000   0.00000   0.0000   0.0000   0.0000   0.0000   0.0000   0.0000   0.0000   0.0000	1.355   1.35	1.355   0.7590   0.0000   0.	1.355   1.35	1.282   1.28	1.000000   1.000000   1.000000   1.000000   1.0000000   1.000000   1.0000000   1.0000000   1.0000000   1.0000000   1.000000000   1.0000000   1.0000000   1.0000000   1.000000   1.000000   1.000000   1.00000   1.00000   1.000000   1.000000   1.00000   1.000000   1.000000   1.000000   1.000000   1.000000	NATIONAL STATE OF THE PROPERTY	COLING CO

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8830308830225555555555555555555555555555

		Table 2.	2.5-B1 (Concluded	luded)			
OBS	ΠD	WWT_AS	WITCD	WWT_CU	WWT_PB	WVT_ZN	V EXT
135	WTK2SCW6P2 WTK2SCW6Q1	0.597	3.1690	46.685	103.639 6.429 17.839	1139.87 301.87	255.8 888
137 137	VIK2SCV9P1 VIKSSCV1OR1	0.361	0.0390	0.512	2.329	205.87 205.87	25.55 25.08 25.08
139 140	VIKSSCV10R3 VIKSSCV10R4	0.525	0.0698	1.595	27.439 36.139	_33.17 49.37	25.01 25.02
141 142	VTKSSCV11R2 VTKSSCV12R1	$0.288 \\ 0.376$	0.0522	0.846 0.922	0.379	7.93 8.16	25.06 25.04
143 144	WTKSSCW8R1 WTKSSCW8R2	1.665 3.565	0.0740	1.575 0.768	0.03	20.77 63.87	25.01 24.96
145	VTKSSCV901	0.278	0.2030	0, 08	50.0	/8.0/	24.99

		Table 2.5-82	ыапк	Analysis			
OBS	Ð	WVT AS	WWT_CD	WWT_CU	WWT_PB	WWT_ZN	
H20	VTBLANKR3 VTBLANKR2	0.000	0.0010	0.008	0.043	0.065	
04v	WIBLANKR9 WTBLANKR8	000 000 000 000 000	0.0001	0.039	0.000	0.00	
9~α	VTBLANKR5 VTBLANKR6 VTRI ANKR7	0000		0000	0.840 1.090 0.110	0.057 0.132 0.430	
oo	INTELLEGISTICS			010	030	0.078	

Table 2.5-B3 Blank Analysis Summary

VARIABLE	z	MEAN	STANDARD DEVIATION	MINIMUM VALUE	MAXIMUM VALUE	STD ERROR OF MEAN	SUM	VARIANCE	C.V.
WWT AS WWT CD WWT CU WWT PB	თთთთ	0.005	0.000	000000000000000000000000000000000000000	0.005	0.000 0.000 0.164 0.164	0.045 0.013 3.251 975	000000000000000000000000000000000000000	172.38 78.83 136.51

Table 2.5-B4 Wet Extraction (June and July 1986)

0BS ID WT\_SE VET CONTROLL

1 VIBLANCES

2 VICESCU26F2

0 VICESCU26F3

0 VICESCU26F3

0 VICESCU27F1

0 VICE

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# 00000000111440100881448100001084448018141000010110000 # 40244188884400888488414481100010884118118118118118118181818
100000110001181111000011900000000000000
00000001111000111101000000000000000000
20000000000000000000000000000000000000
UTAASCU16U5 WTAASCU16U6 WTAASCU16U6 WTAASCU15Q2 WTAASCU15Q2 WTABSCU15SQ2 WTABSCU15SQ3 WTABSCU15SQ3 WTASSCU10Q1DQ1 WTKSSCU10Q1DQ1 WTKSSCU10Q1DQ1 WTKSSCU10Q1DQ1 WTKSSCU10Q2DQ1 WTKSSCU10Q1DQ1 WTKSSCU10Q1DQ1 WTKSSCU10Q1DQ1 WTKSSCU10Q1DQ1 WTKSSCU10Q1DQ1 WTKSSCU10Q1DQ1 WTKSSCU10Q1DQ1 WTKSSCU10Q1DQ1 WTKSSCU10Q1DQ1
00 80 100000000000000000000000000000000

		lable 2.	בייונטט) בפ-כ	(continued)		
BS	ΩI	WWT_AS	WWT_CD	WYT_CU	WWT_PB	WYT ZN
46	VTKSSCV1102D4 VTKSSCV1102D1	9.6949	0.281	27.972 24.672	0.00-	35.27 32.57 55.87
844° 800°	WIKSSCWIIQZDZ WIKSSCWIIQZD3 WIKSSCWIIO2D4	6.1549 6.1549 0.1369	0.414 1.000	43.672 22.072	0.05	79.97 79.97 80.17
222	VIKSSCV1103D1R1 VIKSSCV1103D1R2	5.4749	$0.078 \\ 0.136$	12.572	0.03	7.50 10.37
553	WTKSSCW1103D1R3 WTKSSCW1103D2	5.2949	0.141 0.094	11.272 9.272 9.272	0 0 0 0 0 0 0 0 0	12.37
<b>.</b>	WTKSSCW1103D3 WTKSSCW1103D4	0.5209	0.187	4.952 17.022	1.48	54.47
~85°	WTKSSCW11R4D1 WTKSSCW11R4D2	0.2769	0.953	13.372	000	128.97
, 187	WIKSSCWIIR4US WIKSSCWIIR4D4 WIKSSCWIIIP5D1	0.6429	0.313	0.659	0.10	60.00
7 62 63	WIKSSCW11R5D2	0.1349	0.015	0.288	0.57	1.75
345	WIKSSCW11R5D3R2 WIKSSCW11R5D3R2 UTVSSCW11R5D3R3	0.0569	000	0.190	888	0.00
385	WIKSSCU11R5D4 UTKSSCU11R5D4	0.0689	1.820	0.171	0.12	49.6
286	VTKSSCV11R6D2 VTKSSCV11R6D2	0.6349	2.730	7.702	0.16 0.11	139.97
22.	WIKSSCW11R6D4 WIKSSCW11R7D1	0.1679	$\frac{1.260}{0.170}$	1.252	3.00	33.9
, 72 73	VIKSSCV11R7D2 VIKSSCV11R7D3	0.9759	0.067	0.256	00 88	22.87 42.0 <u>7</u>
7 <u>4</u> 75	VIKSSCV11R7D4 VIKSSCV11R8D1	0.3989 2.4349	0.248 0.087	0.315 9.852	0.04	72.27
<u>),6</u> 77	VIKSSCV11R8D2 VIKSSCV11R8D3	$\frac{1.5749}{0.1939}$	$0.118 \\ 0.132$	18.072 2.832	$0.14 \\ 0.09$	$\frac{10.8}{11.77}$
138 139	VIKSSCV11R8D4 VIKSSCV11R9D1	0.1689 34.0949	0.061 0.214	$\frac{1.152}{16.672}$	00.00	16.37
80	VTKSSCV11R9D2R1 VTKSSCV11R9D2R2	1.0949 2.0949	0.419 0.406	33.872 29.472	0.08 0.07	32.9/ 30.3/
83 83	WTKSSCW11R9D2R3 WTKSSCW11R9D3R1	6.5949 0.5789	0.362 0.470	28.272	000	35.47
84 85	VTKSSCV11R9D3R2 VTKSSCV11R9D3R3	2.7349	0.351	24.8/2	0.00	333 333 366
888 878	WTKSSCW11R9D4 WTKSSCW1201D1 WTKSSCW1201D2	0.9949 $0.1869$ $0.2749$	0.060	21.022 0.731 0.324	000 000 003 003	3.27 3.27
68	WTKSSCW1201D3	0.1429	0.021	0.281	0.42	1.37

	WT_ ZW	00000000000000000000000000000000000000
	WWT_PB	000000000000000000000000000000000000000
(Continued)	WWT CU	00000000000000000000000000000000000000
2.5-B5 (Con	WWT_CD	-0000000000000000000000000000000000000
Table	WWT AS	10000000000000000000000000000000000000
	ID	UTKSSCV1201D4 UTKSSCV12R4D1 UTKSSCV12R4D1 UTKSSCV12R4D2R1 UTKSSCV12R4D2R2 UTKSSCV12R4D2R3 UTKSSCV12R4D3 UTKSSCV12R5D1 UTKSSCV12R5D1 UTKSSCV12R6D1 UTKSSCV12R6D1 UTKSSCV12R6D1 UTKSSCV13R1D1 UTKSSCV13R1D1 UTKSSCV13R1D1 UTKSSCV13R1D2R3 UTKSSCV13R1D2R3 UTKSSCV13R1D2R3 UTKSSCV13R1D2R3 UTKSSCV13R1D4R3 UTKSSCV13R3D1 UTKSSCV13R3D1 UTKSSCV13R3D1 UTKSSCV13R3D2 UTKSSCV13R3D3 UTKSSCV13R3D3 UTKSSCV13R4D2 UTKSSCV13R4D3 UTKSSCV13R4D3 UTKSSCV13R4D3 UTKSSCV13R4D3 UTKSSCV13R4D3 UTKSSCV13R5D1 UTKSSCV13R5D1 UTKSSCV13R5D1 UTKSSCV13R5D3
	OBS	27777777777777777777777777777777777777

_
(Concluded)
2.5-B5 (
Table

WYT_ZN	106 699.97 77.929.901 10.201 1
WWT_PB	0.1022000000000000000000000000000000000
WWT_CU	0.0592 1.5522 1.362222228 1.362222228 1.362222228 1.36222222228 1.36222222228 1.36222222228 1.3622222222228 1.36222222222222222222222222222222222222
WWT_CD	00000000000000000000000000000000000000
WWT_AS	00000000000000000000000000000000000000
ID	VTKSSCVBR3D2 VTKSSCVBR3D3 VTKSSCVBR4D1 VTKSSCVBR4D2 VTKSSCVBR4D3R1 VTKSSCVBR4D3R3 VTKSSCVBR4D3R3 VTKSSCVBR4D3R3 VTKSSCVBQ2D2 VTKSSCVBQ2D2 VTKSSCVBQ2D2 VTKSSCVBQ2D4 VTKSSCVBQ2D4R3 VTKSSCVBQ3D1 VTKSSCVBQ3D1 VTKSSCVBQ3D2 VTKSSCVBQ3D2 VTKSSCVBQ3D4 VTKSSCVBR1D1 VTKSSCVBR1D1 VTKSSCVBR1D1 VTKSSCVBR1D3 VTKSSCVBR1D1 VTKSSCVBR1D3 VTKSSCVBR1D3 VTKSSCVBR1D3 VTKSSCVBR1D3 VTKSSCVBR1D3 VTKSSCVBR1D3 VTKSSCVBR1D3 VTKSSCVBR1D3 VTKSSCVBR1D3 VTKSSCVBR1D3 VTKSSCVBR1D3 VTKSSCVBR1D3 VTKSSCVBR1D3 VTKSSCVBR1D3 VTKSSCVBR1D3 VTKSSCVBR1D3
OBS	11111111111111111111111111111111111111

Table 2.5-B6 Blank Analysis

OBS	ID	WWT_AS	WAT CD	WWT_CU	WWT_PB	WZ_TWV
<b>←</b> (	TBLANKR1	0.005	0.0001	0.030	0.00	0.030
7m	WIBLANKRI WIBLANKRII	000	000	0.00	38	000
41	WTBLANKR12	0.005	0.0001	0.030	0.003	0.077
<b>^</b>	VIBLANKRI 3		000.0	0.00	0.00	0,000
٥٢	WIBLANKRI4 UTBLANKRI5	96	0.0001	0.00	100	
- ∞	WTBLANKR2	0.00	0.0001	0.030	0.003	0.015
6	WTBLANKR3	0.005	0.0001	0.030	0.019	0.030
10	VTBLANKR4	0.005	0.0001	0.030	0.013	0.030
Ħ	WTBLANKR5	0.005	0.0001	0.030	0.001	0.030
12	WTBLANKR6	0.005	0.0001	0.030	0.00	0.030
13	VTBLANKR7	0.005	0.0001	0.030	0.001	0.030
14	VTBLANKR8	0.005	0.0001	0.030	0.005	0.030
15	VTBLANKR9	0.005	0.0001	0.030	0.088	0.030

Table 2.5-B7 Blank Analysis Summary

VARIABLE	z	MEAN	STANDARD DEVIATION	MINIMUM VALUE	MAXIMUM VALUE	STD ERROR OF MEAN	SUM	VARIANCE	C.V.
WYT AS WYT CU WYT CU WYT PB	22255 2525 2525 2525 2525 2525 2525 25	0.0051 0.0003 0.0282 0.0100 0.0321	0.0003 0.0007 0.0222 0.0130	0.0050 0.0001 0.0010 0.010	0.0060 0.0027 0.0300 0.0880 0.0770	0.0001 0.0002 0.0018 0.0057 0.0034	0.0760 0.0041 0.4230 0.1500 0.4820	0.00000007 0.00000045 0.0004860 0.00049429 0.00016898	5.096 245.604 24.721 222.325 40.454

## 2.5.10.3 Tables C1-C10 Sample ID and Variable Description

Tables 2.5-C1-C10 present the EP toxicity analysis data. The samples that appear in Tables C1 and C4 were collected in June and July 1986. Samples listed in Table C7 were collected in December 1986. Samples listed in Table C10 were collected in March 1987.

## Variable Description

#### Unit

WWT\_AS, VWT\_CD, mg/l wet weight basis
WWT\_CU, WWT\_PB, WWT\_ZN
EP\_AS, EP\_CD, EP\_PB
SOLID Percent solids
WT Grams
DEPTH Feet

#### Example Key

ID No.: EP AA SCW5T2R1 EP - Extraction Procedure of RCRA used for analysis AA - Sample site area AA: Allied A AB: Allied B CP: Coke pile site ES: ESI G1: G-1 Getty K2: K-2 KS: Kiln site SC - Sample type SC: Soil core GT: Surface sample gritty material RB: Surface sample red brick YB: Surface sample yellow brick W5T2R1 - Specific WES sample site location 5T2 Label for site R1, R2, R3 Triplicate samples Samples IDs in Table C7 included D1-D4. D1-D4 refer to the depth of core: D1 0" - 6" D2 6" - 12" 12" - 24" D3

24" - 36"

D4

Samples IDs in Table C10 included D1-D6.

D1-D6 refer to the depth of core:

D1 0' - 1'

D2 1' - 2' D3 2' - 3' 3' - 4' **D4** 4' - 5' 5' - 6' D5 D6

- Sample taken June 24, 1986 Sample taken June 25, 1986
- Resample previous contractor site

	TA	00000000000000000000000000000000000000
(98)	WYT ZN	23 23 24 25 25 25 20 20 20 20 20 20 20 20 20 20 20 20 20
and July 19	WWT_PB	
Table 2.5-C1 EP Toxicity (June and July 1986)	WATCH	00000000000000000000000000000000000000
	WWT_CD	00000000000000000000000000000000000000
	WVT_AS	
	ID	EPAASCU12V2 EPAASCU14X2 EPAASCU16V1 EPAASCU16V4 EPAASCU16V4 EPASCU16V1 EPCPSCU26F1 EPCPSCU26F3 EPCPSCU26G3 EPCPSCU26G3 EPCPSCU29E10 EPCPSCU29E11 EPCPSCU29E11 EPCPSCU29E1 EPCPSCU20E1
	OBS	4448838838828828282828282828288384888488

	W	0.000000000000000000000000000000000000
	WZ_TWW	11.15555555555555555555555555555555555
	WWT_PB	00000000000000000000000000000000000000
2.5-C1 (Concluded)	WWT_CU	0.000000000000000000000000000000000000
Table 2.5-C1 (	WWT_CD	00000000000000000000000000000000000000
Tab	WWT_AS	
	ΩI	EPGISCU13L5 EPGISCU13M1 EPGISCU13M5R1 EPGISCU13M5R2 EPGISCU13M5R3 EPGISCU14L2R3 EPGISCU14L2R3 EPGISCU14L2R3 EPGISCU14L2R3 EPGISCU10P2 EPK2SCU3R1 EPK2SCU3R1 EPK2SCU403 EPK2SCU403 EPK2SCU403 EPK2SCU403 EPK2SCU403 EPK2SCU403 EPK2SCU6P2 EPK2SCU6P2 EPK2SCU6P2 EPK2SCU6P2 EPK2SCU6P2 EPK2SCU6P2 EPK2SCU6P2 EPK2SCU6P2 EPK2SCU6P2
	OBS	44444444444444444444444444444444444444

	_		
	WWT_PB	0.002	
	WATE CU	0.002	
Analysis	WWT CD	0.0008	
Table 2.5-C2 Blank Analysis	WWT_AS	0.005	
Table	OI (I	EPBLANKR1 EPBLANKR2	
	OBS	7	

Table 2.5-C3 Blank Analysis Summary

VARIANCE C.V.	00 0.0000 0.000 09 0.0000 109.994 30 0.0000 47.140 30 0.0000 47.140 10 0.0267 112.262
SUM	20000
STD ERROR OF MEAN	000000000000000000000000000000000000000
MAXIMUM VALUE	0.0050 0.0020 0.0020 0.2610
MINIMUM VALUE	0.0000000000000000000000000000000000000
STANDARD DEVIATION	0.0000 0.0005 0.0007 0.1633
MEAN	0.0050 0.00050 0.0015
z	22222
VARIABLE	WWT AS WWT CD WWT PB

Table 2.5-C4 EP Toxicity (June and July 1986)

20:10:00:04:1:10:00:00:00:00:00:00:00:00:00:00:00:0
00000000000000000000000000000000000000
00000000000000000000000000000000000000
00000000000000000000000000000000000000
AT AS SECOND 000000000000000000000000000000000000
EPAASCU10R2 EPAASCU10R2 EPAASCU10S2 EPAASCU10S2 EPAASCU10T1R1 EPAASCU10T1R3 EPAASCU11R1R1R2 EPAASCU11R1R3 EPAASCU11R1R3 EPAASCU11R1R3 EPAASCU11R1R3 EPAASCU11R1R3 EPAASCU16U3 EPAASCU16W3 EPAASCU16W3 EPAASCU16W3 EPAASCU16W3 EPAASCU16W3 EPAASCU16W3 EPAASCU16W3 EPASCU16W3 EPASCU16W3 EPASCU16W3 EPASCU16W3 EPASCU16W3 EPASCU16W3 EPASCU14W3 EPABSCU14W3 EPABSCU14W3 EPABSCU14S1 EPABSCU15S1 EPABSCU15S1 EPABSCU15S1
0 8 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7

Table 2.5-C4 (Concluded)	WWT_AS WWT_CD WWT_CU WWT_PB WWT_ZN WI	0.969 0.950 0.951 0.860 0.951		0.0000 0.0000 0.0000 0.0000 0.0000 0.0005 0.0000 0.0005 0.0000 0.0005 0.0005	0.0015 0.0058 0.030 0.032 0.0015 0.0118 0.014 0.296 0.0010 0.0000 0.028 0.752	000 0.0010 0.0018 0.024 2.839 000 0.0010 0.0048 0.010 0.776 000 0.0035 0.0000 0.010 2.479 000 0.0035 0.0088 0.026 25.569	0.0300 0.0098 0.046 18.569 0.0695 0.0398 0.580 52.669 0.0015 0.0048 0.016 0.740	0.0020 0.0008 0.006 0.070 0.0000 0.0000 0.002 3.299 0.0000 0.0000 0.008 7.239	133 0.0136 0.0638 0.024 6.219 021 0.0021 0.0398 0.092 2.539 009 0.0036 0.0578 0.022 1.429	0.0000 0.02/8 0.004 0.004 0.0000 0.1458 0.044 1.979 0.0035 0.044 1.979
2.5-C4	AS WWT	0000	04 <b>~</b> m0	2000 2000 2000 2000	0000 0000	300c	8000 8000	000	133 0021 009 000 000	0020
	OI OI	3PCPSCW29E11R2 3PCPSCW29E11R3 3PCPSCW29E2R2 3PCPSCW29E2R2	EPCPSCW29F3R1 EPCPSCW29F3R1 EPCPSCW29F3R3 EPCPSCW30F1	GPCPSCW30F4A1 GPCPSCW30F4R2 GPCPSCW30F4R3 GPESSCW13H1	EPESSCV13H2 PESSCV13J1 PESSCV13J1	PESSCW13J2 PESSCW13J3 PESSCW13K1	IPESSCVI 3K2R2 IPESSCVI 3K2R3 IPESSCVI 3K3	IPESSCV14F1 IPG1SCV12N2A IPG1SCV12N2B	EPKSSCV10R1 EPKSSCV10R3 EPKSSCV10R4	EPKSSCW11R1 EPKSSCW8R1 EPKSSCW8R3
	S		70H06							

	Table 2.5-C5 Blank	5 Blank Ana	Analysis		
E	WWT_AS	WWT_CD	war_cu	WWT_PB	WYT ZN
EPBLANKR3	0.005	0.0027	0.001	0.002	0.032
EPBLANKR5	0.000	000.0	0.001	0.00	0.030
EPBLANKR6	0.00	0.0001 0.0001	0.001 0.001	0.001	0.030
CPBLAINKK/			35	7000	0.03

Table 2.5-C6 Blank Analysis Summary

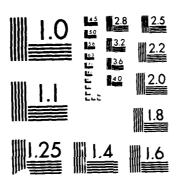
VARIABLE	z	MEAN	STANDARD DEVIATION	MINIMUM VALUE	MAXIMUM VALUE	STD ERROR OF MEAN	MUS	VARIANCE	C.V.
WWT AS WWT CU WWT PB WWT ZN	०००००	0.0050 0.0005 0.0032 0.0017	0.0000 0.00011 0.00053 0.0013	0.0000 0.0001 0.0010 0.0010	0.0050 0.0027 0.0027 0.0330	0.0000 0.00024 0.00224 0.00224	0.0300 0.0032 0.0190 0.0100	00000	0.000 199.021 167.597 30.984

	WYT ZN	34222862000000000000000000000000000000000
(9	WWT_PB	000000000000000000000000000000000000000
(December 1986)	WWT_CU	00000000000000000000000000000000000000
Toxicity (De	WATCD	00000000000000000000000000000000000000
2.5-C7 EP To	WWT_AS	000000000000000000000000000000000000000
Table 2	ID	EPAASCU16U8 EPABSCU1502R1 EPABSCU1502R2 EPABSCU1502R3 EPABSCU1502R3 EPABSCU1553 EPABSCU1553 EPABSCU1553 EPABSCU1553 EPASSCU1001D1 EPKSSCU1001D1 EPKSSCU1002D1R1 EPKSSCU1002D1R2 EPKSSCU1002D1R2 EPKSSCU1002D1R3 EPKSSCU1003D1 EPKSSCU1003D1 EPKSSCU1003D2 EPKSSCU1003D2 EPKSSCU1003D3 EPKSSCU1003D3 EPKSSCU101D3 EPKSSCU101D3 EPKSSCU1101D3 EPKSSCU1101D3 EPKSSCU1101D3 EPKSSCU1101D3 EPKSSCU1101D3 EPKSSCU1101D3 EPKSSCU1101D3 EPKSSCU1101D3 EPKSSCU1102D3
	OBS	28232222222222222222222222222222222222

Table 2.5-C8 Blank Analysis

WWT_PB	000
WWT_CU	0003
WWT_CD	0.0000
WWT AS	0000
ID	BLANKR1 BLANKR2 RLANKR3

REMEDIAL INVESTIGATION OF CONTAMINANT MOBILITY AT NAVAL MEAPONS STATION C. (U) ARMY ENGINEER MATERMAYS EXPERIMENT STATION VICKSBURG MS ENVIR. CR LEE ET AL. JUN 88 MES/MP/EL-86-2-APP F/G 24/4 AD-R195 946 2/2 UNCLASSIFIED



UTION TEST CHART

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Table 2.5-C9 Blank Analysis Summary

C.V.	0.000 154.649 21.651 125.967 40.733
VARIANCE	0.00000000 0.00002500 0.00000333 0.000021333
SUM	0.01500000 0.00970000 0.00800000 0.01100000
STD ERROR OF MEAN	0.00000000 0.00288694 0.00033333 0.00266667
MAXIMUM VALUE	0.0050000000000000000000000000000000000
MINIMUM VALUE	0.00500000 0.00010000 0.00200000 0.00100000
STANDARD DEVIATION	0.00000000 0.00500033 0.0057735 0.00661880
MEAN	0.0050000 0.00323333 0.00266667 0.00366667
z	നനനന
RIABLE	WYT AS WYT CU WYT CU

	SOLID	8888666688872288888666888832566888888888888888888888
1987)	EP_PB	88988888888888888888888888888888888888
ty (March	EP_CD	000000000000000000000000000000000000000
EP Toxicity	EP_AS	000000000000000000000000000000000000000
Table 2.5-C10	П	KSSCW1100151 KSSCW110100251 KSSCW110100151 KSSCW110100151 KSSCW110100551 KSSCW110100551 KSSCW110110551 KSSCW110110551 KSSCW110110551 KSSCW110110551 KSSCW110120551 KSSCW110120551 KSSCW11040551 KSSCW11040551 KSSCW11040551 KSSCW11050551 KSSCW11050551 KSSCW11050551 KSSCW11050551 KSSCW11060551
	DEPTH	000HQM4N0HQM4N0HQM4N0HQM4N0HQM4N0HQM4 
	S	OHOR45997890HOM45997890HOM4599789

DEPTH	a	EP_AS	EP_CD	EP P
010m4v0010m4v0 15-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-	KSSCV1108D1S1 KSSCV1108D2S1 KSSCV1108D4S1 KSSCV1108D4S1 KSSCV1108D6S1 KSSCV1109D2S1 KSSCV1109D2S1 KSSCV1109D4S1 KSSCV1109D4S1 KSSCV1109D6S1 KSSCV1109D6S1	000000000000000000000000000000000000000	000000000000000000000000000000000000000	000000000000000000000000000000000000000
	DEPTH 10-1 10-1 10-1 10-1 10-1 10-1 10-1 10-	TO TO THE	EP KSSCV1108D1S1 0.12 KSSCV1108D1S1 0.12 KSSCV1108D2S1 0.13 KSSCV1108D5S1 0.13 KSSCV1108D6S1 0.13 KSSCV1109D1S1 0.2 KSSCV1109D4S1 0.2 KSSCV1109D4S1 0.2 KSSCV1109D6S1 0.2 KSSCV1109D6S1 0.2 KSSCV1109D6S1 0.13 KSSCV1109D6S1 0	EP_AS EF KSSCV1108D1S1 0.28 0. KSSCV1108D2S1 0.16 0.16 0.16 0.16 0.16 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19

## 2.5.10.4 Tables D1-D16 Sample ID and Variable Description

Tables D1-D8 contain clam tissue analysis. The samples that appear in Table D1 were collected in June 1986.

#### Variable Description

CONTRACTOR OF THE STREET OF SAFETY O

Unit

AS,CD,PB,ZN

mg/kg or parts per million(ppm)

dry weight basis

VOLUME

Milliliters(ml)

CLAM IN, CLAM OUT

Integer

DRYWT

Grams

## Example Key

ID No.: AB CL W12S1R3

AB - Sample site area

AA: Allied A

AB: Allied B

BK: Remote reference site

ES: ESI

G1: G-1 Getty

K2: K-2

CL - Sample type

CL: Clam tissue sample

W12S1R3 - Specific WES sample site location

12S1 Label for site

R1, R2, R3 Triplicate samples

	CLAM_IN	ないというないというないというないというないというないというないというないとい
1986)	VOLUME	SOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOO
	CLAM_OUT	2222222222222222222222222222222222222
ysis (June	DRYVT	
Table 2.5-D1 Clam Tissue Analysis	ZN	222239963322288011222222222222222222222222222222
	PB	000000000000000000000000000000000000000
	8	88928888888888888888888888888888888888
	AS	22222222222222222222222222222222222222
	TD OI	AACLUIORSRI AACLUIORSRI AACLUIORSRI AACLUIOSRI AACLUIOTIRI AACLUI241RI AACLUI242RI AACLUI242RI AACLUI244RI AACLUI244RI AACLUI244RI AACLUI246RI AACLUI246RI AACLUI246RI AACLUI246RI AACLUI246RI AACLUI246RI AACLUI248RI AACLUI248RI AACLUI243RI AACLUI2VIRI AACLUI2VIRI AACLUI2VIRI AACLUI2VIRI AACLUI2VIRI AACLUI2VIRI AACLUI2VIRI AACLUI2VIRI AACLUISUIRI AACLUISUIRI AACLUISUIRI AACLUISUIRI AACLUISUIRI AACLUISUIRI AACLUISUIRI AACLUISUIRI AACLUISUIRI AACLUISUIRI AACLUISUIRI AACLUISUIRI AACLUISUIRI AACLUISUIRI AACLUISUIRI AACLUISUIRI AACLUISUIRI AACLUISUIRI AACLUISUIRI

	CLAM_IN	<u> </u>
	VOLUME	SONONONONONONONONONONONONONONONONONONON
	CLAM_OUT	なみられななおおおおおおおおおおおおおおおおおおおおおおおおおおおおおおおおおお
nded)	DRYWT	00000000000000000000000000000000000000
5-Table 2.5-D1 (Concluded)	NZ.	082820111020222222222222222222222222222
	PB	00000000000000000000000000000000000000
Table 2.	8	ることできることでは、これできます。これでは、これでは、これでは、これでは、これでは、これでは、これでは、これでは、
	AS	22222222222222222222222222222222222222
	CI CI	AACLU6SIR3 AACLU6SIR3 AACLU6SIR3 AACLU7SIR3 AACLU7IR12 AACLU7IR12 AACLU7IR12 AACLU7IR13 AACLU7IR13 AACLU7IR13 AACLU7IR13 AACLU8S2R3 AACLU8S2R3 AACLU8S2R3 AACLU8S2R3 AACLU8V2R1 AACLU8V2R3 AACLU8V2R1 AACLU8V2R3 AACLU8V3 AACLU8V
	OBS	74407727377777762828288888888888888888888888

Table 2.5-D2 Blank Analysis

PB ZN	0.007 0.006 0.006 0.003 0.006 0.007 0.006 0.007 0.006 0.007 0.006 0.007 0.006 0.007 0.006 0.007
8	
AS	00000000000 80000000000000000000000000
OI	NVSCLWBLKR1 NVSCLWBLKR2 NVSCLWBLKR4 NVSCLWBLKR5 NVSCLWBLKR6 NVSCLWBLKR6 NVSCLWBLKR7 NVSCLWBLKR7 NVSCLWBLKR7 NVSCLWBLKR9 NVSCLWBLKR9 NVSCLWBLKR9 NVSCLWBLKR9
OBS	10 10 11 11

Table 2.5-D3 Blank Analysis Summary

ر. د.	0.0 0.0 67.8 133.9
VARIANCE	000000000000000000000000000000000000000
MOS	0.0550 0.0011 0.0640 2.1650
STD ERROR OF MEAN	0.0000 0.0000 0.0012 0.0795
MAXTMUM VALUE	0.0050 0.0001 0.0160 0.9850
MINIMUM VALUE	0.0050 0.0001 0.0710
STANDARD DEVIATION	0.0000 0.0000 0.0039 0.2637
MEAN	0.0050 0.0001 0.0058 0.1968
z	
VARIABLE	SBCB SBCB SBCB SBCB SBCB SBCB SBCB SBCB

	DRYVT	0.000000000000000000000000000000000000
arysis	ZZ	743.6 760.8 760.8 777.6 739.1 765.7 765.7 765.7
lable 2.3-D4 NBS Standard Analysis	PB	000001100000 44761800000
CSN PU-C	8	######################################
lable 4	AS	25555555555555555555555555555555555555
	Ω	NWSCLWOYSR1 NWSCLWOYSR3 NWSCLWOYSR3 NWSCLWOYSR6 NWSCLWOYSR6 NWSCLWOYSR7 NWSCLWOYSR8 NWSCLWOYSR8 NWSCLWOYSR8 NWSCLWOYSR10 NWSCLWOYSR10
	OBS	110 110 110

Table 2.5-D5 NBS Standard Analysis Summary

c.v.	7.937 9.800 70.234 2.025 11.003						
VARIANCE	0.0210 0.1120 0.2307 240.4595 0.0037						
NUS	20.1017 37.5654 7.5219 8422.1892 6.1130						
STD ERROR OF MEAN	0.0437 0.1009 0.1448 4.6755 0.0184						
MAXIMUM VALUE	2.1168 3.8668 1.7949 789.2702 0.6850			15.3	3.9	0.52	866.0
MINIMUM VALUE	1.5924 2.8501 0.0000 738.9873 0.4710		Ø	11.5	3.1	0.44	838.0
STANDARD DEVIATION	0.1450 0.3347 0.4803 15.5068 0.0611		Tissue Analysis Values				
MEAN	1.8274 3.4150 0.6838 765.6536 0.5557		Tissue Ana				
z		lards	NBS Oyster				
VARIABLE	AS CD III ZN III DRYWT	*Standards	NBS (	AS	8	PB	ĸ

Table 2.5-D6 Initial Clam Tissue Analysis

	DRYVT	0.502000 0.586000 0.508000
	ZN	87.9681 94.9829 92.8346
•	PB	0.418327 0.443686 0.413386
	8	2.38048 2.03925 2.45079
	AS	1.49402 1.45051 1.57480
	ID	NWSCLVBKGCLMR1 NWSCLVBKGCLMR2 NWSCLVBKGCLMR3
	S	

			Table 2.	Table 2.5-D/ Initial	Clam	Tissue Analysi	is Summary		
ARIABLE	z	MEAN	STANDARD DEVIATION	MINIMUM VALUE	MAXIMUM VALUE	STD ERROR OF MEAN	NOS	VARIANCE	C.V
AS CD PB ZN DRYVT	നനനന	1.5064 2.2902 0.4251 91.9286 0.5320	0.0631 0.2201 0.0163 3.5941 0.0469	1.4505 2.0392 0.4134 87.9681 0.5020	1.5748 2.4508 0.4437 94.9829 0.5860	0.0364 0.1271 0.0094 2.0751 0.0271	4.5193 6.8705 1.2754 275.7857 1.5960	0.0040 0.0485 0.0003 12.9176 0.0022	4.0.5.08 9.0.80 8.0.00 8.0.00 8.000

NZW	384 43 1993.05 144 43 1115.243 JKHH 1175.243 JKHH 1735.111 ORPAN 1735.13 JKHH 1735.13 JKH 1735.13 J
MPB	00000000000000000000000000000000000000
<del>0</del>	######################################
MAS	2.39 EIFHG 22.39 EID FHG 23.39 EID
А	AACIMIORS AACIMIORS AACIMI2443 AACIMI2445 AACIMI2446 AACIMI2446 AACIMI2446 AACIMI2446 AACIMI241 AACIMI241 AACIMI241 AACIMI332 BRCCM1161 BRCCM1161 BRCCM1261 BRCCM1331 ESCOM1341 ESCOM1341

Table 2.5-D9 Summary of Field-Collected Water Quality Data

Day 1 (21–22 May 86) AREA PH
8.2 (7.8-8.5)
7:7 (7.5-7.9)
$\binom{8.1}{8.1-8.1}$
8.0 (7.9-8.0)
7,7 (7.2-8.5)
7,4(7.4-7.4)
DAY 28 (18-19 JUNE 86)
H.
6.8 (6.8-6.8)
7.4 (7.3-7.5)
7.0 (7.0-7.0)
7,4 (7.1-7.8)
7.8 (6.8-8.4)
6.9 (6.9-6.9)

Table 2.5-D10 Condition Index Corbicula fluminea for Concord Naval Weapons Station

AA12S1 19 Jun 86 (Field)	7.30 8.89 8.85 11.68 7.64 9.36 6.87 12.51 8.08 8.18 7.57 8.61 9.91 8.34 9.22 9.72 7.38 7.09 7.29 9.81 7.67 10.70 10.73 10.47 8.78 11.55 9.54 11.73 10.12 11.94 8.83 8.34 10.65 9.85 BCD AB	
AA10S3 18 Jun 86 (Field)	7.30 8.85 7.64 6.87 8.08 7.57 9.91 no clam 9.22 7.29 7.29 7.29 7.29 7.29 7.27 10.73 8.78 9.54 12.75 7.76 10.12 8.83 10.65 10.65 10.65	
AA6S1 18 Jun 86 (Field)	9.33 5.02 9.01 8.74 8.74 8.01 10.43 9.11 8.70 11.13 10.40 7.28 7.10 10.73 9.58 11.24 7.30 13.99 10.16	
AA7T3 18 Jun 86 (Field)	8.16 9.33 9.69 5.02 10.69 9.01 7.10 8.74 10.64 8.55 6.11 9.94 7.82 8.01 7.84 10.43 9.32 9.11 8.84 8.70 7.52 11.13 10.18 10.40 6.90 7.28 8.48 7.10 11.30 10.73 10.47 9.58 10.67 7.30 9.40 13.99 9.40 13.99 9.45 10.16	
AA12V1 19 Jun 86 (Field)	8.05 9.91 10.92 7.84 8.93 6.63 9.25 9.30 8.24 8.71 10.87 8.60 10.68 9.61 11.32 8.83 6.99 10.45 10.45 10.88	
AA124,6 18 Jun 86 (Field)	9.57 11.54 10.49 12.94 9.11 8.39 9.16 7.95 10.15 11.13 9.85 9.79 11.18 9.71 10.16 6.10 11.12 10.16 6.10	
BK116,1 18 Jun 86 (Field)	9.96 6.99 9.66 8.63 7.80 10.39 8.91 8.91 8.91 8.48 11.39 7.49 9.61 8.39 9.92 11.18 10.07 8.90 8.90 8.90	
BKGD, 2 18 Jun 86 (Lab)	5.86 6.07 6.82 7.30 7.46 6.18 6.18 5.02 5.93 5.02 5.15 6.13 5.12 5.12 5.12 5.12 6.13 5.14 6.13 6.13 6.13 6.13 6.13 6.13 6.13 6.13	
BKGD,1 21 May 86 (Lab)	6.71 8.86 8.83 9.58 7.22 7.24 7.92 7.92 7.18 7.18 6.38 6.38 7.31 5.62 7.37 8.21 7.37 8.21	
Sample	X 20	

Samples with the same letter are not significantly different at the P = 0.05 level.

Table 2.5-D10 (Concluded)

BK133,2 19 June 86	(Field)	5.86 7.02 8.61 7.46 8.57 7.54 8.57 10.02 11.91 8.55 13.47 9.08	6.92 8.74±1.76 BCD	
ES13J1 19 June 86	(Field)	8.90 10.67 2.77 7.27 7.27 7.50 10.16 8.10 8.10 8.50 13.09	7.89 8.15 <u>+</u> 1.99 DE	
ES13L1 19 June 86	(Field)	6.13 6.55 6.30 6.30 7.34 7.87 7.87 7.70 8.18 8.37 8.37 8.37	7.12 7.22 <u>+</u> 1.52 F	
G112N2 9 June 86	(Field)	9.80 8.37 7.68 7.50 7.50 7.23 7.23 8.83 8.83 9.12 9.77	7.71 8.40 <u>+</u> 1.29 CDE	
	Sample	1 2 4 3 7 6 10 11 12 11 13 14 11 16 11 19 19	20 <b>X</b> <sup>2</sup>	

Table 2.5-D11 Clam Biomonitoring Metal Concentrations (mg/kg, dry wt basis)

Field	From Lit.	4.60 - 7.10*	0.00 - 6.00**		110 - 349**	
	1986 Min-Max	1.5 - 3.0 (14)+	1.7 - 3.9 (6)	0.0 - 8.7 (2)	93.8 - 404 (14)	
	1984 Min-Max	0.86 - 2.59 (0)+	0.02 - 2.71 (3)	0.00 - 9.21(4)	99.9 - 284 (6)	
,	Metal	As	ਝ	Pb	Zn	

The number of sites with tissue concentrations statistically above background (BK1332, BK1161 or BK1162). Rodgers et al. 1980. Luoma, Cascos, and Dagovitz 1984.

Table 2.5-D12 Field Measurements for Kiln Site Monitoring Wells (May and August 1987)

		}	May 17	May 12, 1987		
		Water*			Temperature	
Sample	Time	Level (ft)	핍	Conductivity (umhos)	(°F)	
Field Blank	1030	1	7.16	12	78.8	
Background well	1045	41.0	7.35	1513	74.6	
KS-1	1130	4.5	7.3	>20000	74.6	
KS-2	1255	4.9	7.7	7520	74.4	
KS-3	1400	5.1	7.3	4220	73.9	

			August 1	8, 1987		
Sample	Time	Water* Level (ft)	띲	Conductivity (umhos)	Temperature (°F)	Salinity (ppt)
Field Blank	0845	ı	5.6	-	72.5	0
Background well	0060	41.5	7.2	1280	66.2	<b>—</b>
KS-1	1045	4.9	7.1	18000	68.0	12
KS-2	1230	5.4	7.35	6500	73.4	7
KS-3	1300	5.5	7.15	3800	8.69	2.5

 $<sup>\</sup>star$  Water levels were measured from the top of the PVC casing.

Table 2.5-D13 Well Development Soil and Ground-water Analysis Metal Concentration (mg/kg or mg/l)

		melal W	metal Concentration (mg/kg of mg/l)	(***8/ K&	Of #8/1)	
Soil Sample	Arsenic	Cadmium	Lead	Copper	Zinc	Selenium
Tota	Total Threshold Limit Concentration (TTLC) (mg/kg)	Limit Conc	entration	(TTLC) (I	ng/kg)	
10	77	1:1	, 20 , 20	19	38	0.59
WB - 2 - 4/2/8/ WB - 3 - 4/2/87	55 55	1.3	4.3 15	17	8 4	0.71
TTLC Criteria	200	100	1,000	2,500	2,000	100
	EP Toxicity (mg/l)	(mg/1)				
WB - 1 - 4/2/87 WB - 2 - 4/2/87 WB - 3 - 4/2/87	0.12 0.13 0.17	0.01 0.01 0.01	0.05 0.05 0.09			
EP Toxicity Criteria:	5.0	1.0	10			
	Ground-water Samples (mg/l)	Samples (	mg/1)			
*DWB 5/12/87 (unfiltered) +SWB 5/12/87 (unfiltered)	<0.005 0.110	0.009	0.088	0.087	0.030	0.007
EPA Drinking Water Quality Criteria	0.05	0.010	0.05	1.0	5.0	0.01
EPA Water Quality Criteria (chronic) Freshwater Saltwater	0.190	0.0011	0.0032	0.012	0.047	0.035

<sup>\*</sup> Water collected during the development of the wells. + Water collected during the bailing out of the wells.

Table 2.5-D14 Water Sample Analysis (May 1987)

Background	Unfiltered	<0.005	<0.005	0.055	0.058	0.046	<0.005
	Filtered	<0.005	0.00	0.020	0.080	0.046	<0.005
Field Blank	Unfiltered	<0.005	<0.005	0.050	0.044	0.020	<0.005
KS-3	Unfiltered	0.014	0.0078	0.20	0.084	0.18	<0.005
<b>×</b>	Filtered	<0.005	0.012	0.030	0.11	0.077	<0.005
KS-2	Unfiltered	<0.007	0.0086	0.040	0.084	0.092	<0.005
×	Filtered	<0.011	<0.005	0.020	0.064	0.087	<0.005
KS-1	Unfiltered	<0.005	0.016	0.080	960.0	0.32	<0.005
	Filtered	<0.005	0.026	0.040	0.14	0.16	<0.005
	Metal (mg/l)	As	3	Zn	Pb	ಸ	Se

Table 2.5-D15 Water Sample Quality Control Data (May 1987)

		Duplicate I	Duplicate II	Spike Solution Added	Spiked Sample	% Recovery
				(mg/l)		
Zh	001	090.0	0.050	1.45	1.40	92.7
Pb		0.048	0.068	1.45	1.38	92.6
3	100	<0.005	<0.005	1.45	1.30	9.68
ಬ	001	0.036	0.056	1.45	1.31	87.2
As		<0.005	<0.005	0.05	0.044	88.0
Se	003	<0.005	<0.005	0.05	0.051	102

Table 2.5-D16 Water Sample Analysis (August 1987)

	ltered	11	35	)1	22
round	Unfil	<0.01	<0.05	0.01	0.05
Background	Filtered <0.01	<0.01	<0.05	0.0072	0.020
Blank	Unfiltered <0.01	<0.01	<0.05	0.015	<0.01
Field Blank	Filtered <0.01	<0.01	<0.05	0.0055	<0.01
<sub>ن</sub>	Unfiltered 0.013	0.020	090.0	0.014	0.020
KS-3	Filtered 0.014	<0.01	090.0	0.016	0.020
.2	Unfiltered 0.023	0.020	0.080	0.044	0.030
KS-2	Filtered 0.021	0.015	0.070	0.42	0.020
5-1	0.051 0.057 0.021 0.023 0.014 0.013 <a href="https://doi.org/10.023">Kiltered Willtered Wiltered Wiltered Wiltered Wiltered Wiltered Wiltered O.01</a>	0.040	0.12	0.24	0.050
KS-1	Filtered 0.051	0.030	0.10	0.23	0.030
	Metal As	3	Zn	Pb	ਹ

Note: All metal concentrations are mg/l.

<0.01

<0.01

<0.01

<0.01

0.015

0.015

0.015

0.015

0.034

Se

## 2.5.10.5 Sample Survey Measurements, Table E1

Table 2.5-E1 Sample Survey Measurements

SITE	DISTANCE FT.	BEARING DEG. MIN. SEC.
CPSCW27E2 CPSCW27E2 CPSCW27E3 CPSCW29E10 CPSCW29E11 CPSCW29E12 CPSCW30F4 K2SCW30F3 K2SCW4P2 K2SCW3P2 K2SCW3P2 K2SCW3P3 K2SCW3P1 K2SCW3P1 K2SCW1001 K2SCW1001 K2SCW1001 K2SCW10N2 K2SCW10N2 K2SCW10N3 K2SCW10N3 K2SCW10N3 G1SCW12M4 G1SCW12M4 G1SCW12M4 G1SCW12M5 G1SCW12M6 G1SCW12M6 G1SCW14M3 G1SCW14N3 G1SCW14N2 G1SCW14N3 G1SCW14N2 G1SCW14M3 AASCW16X6 AASCW16X6 AASCW16X5 AASCW16X5 AASCW14X1	DISTANCE FT	
AASCW12W2 AASCW10S1 AASCW10S2 AASCW5R2 AASCW7T2 AASTW7T3	948.75 736.65 1834.50 1703.79 1681.53	353

Table 2.5-E1 (Continued)

SITE	DISTANCE FT.	BEARING DEG. MIN. SEC.
SITE	FT	DEG. MIN. SEC.  299 57 10  308 07 18  318 15 24 55  319 16 18  286 20 55  279 43 50  303 13 35  262 25 55  279 43 30  303 13 35  278 15 39  278 15 39  278 286 20 55  278 286 20 55  278 286 20 55  278 286 20 55  278 286 20 55  278 286 20 55  279 42 22  286 244 25 10  240 44 25  240 00 00  240 44 25  250 06 52 18  247 47 25  250 06 52 18  261 48 21  250 06 256  261 48 21  275 02 18  265 40 40 20  277 02 41
KSSCW13R4 KSSCW12R5 KSSCW11R5	346.94 441.98 538.69	259 37 22 265 07 15 269 12 38

Table 2.5-E1 (Concluded)

SITE	DISTANCE FT.	BEARING DEG. MIN. SEC.
KSSCW11R4 KSSCW11R8 KSSCW11R9 KSSCW12R4 KSSCW15S3 KSSCW11Q4 KSSCW11Q5 KSSCW11Q6 KSSCW11Q7 KSSCW11Q8 KSSCW11Q9 KSSCW11Q10 KSSCW11Q11 KSSCW11Q11 KSSCW11Q12 ESSCW13L6 G1SCW14L3 G1SCW14L3 G1SCW14L2 G1SCW14L2 G1SCW13M5 G1SCW12L2 G1SCW13M5 G1SCW12M6 G1SCW12M6 G1SCW13M5 G1SCW12M6 G1SCW13M5 G1SCW12M6 G1SCW13M5 G1SCW12M6 G1SCW13M5 G1SCW13M5 G1SCW12M6 G1SCW13M5 G1SCW10M2 K2SCW502 AASCW16U6 AASCW16U6 AASCW16U6 AASCW16U6 AASCW16U7 AASCW16U5 AASCW16U7 AASCW15S2 AASCW15S2 AASCW15S2 AASCW15S2 AASCW15S2 AASCW15S2 AASCW15S2 AASCW15Q2 WELL 1 WELL 2	850.86 786.71 683.67 683.67 683.65 343.23 817.56 788.82 744.21 780.83 815.71 844.02 868.77 841.10 766.23 251 231 199 363 238 168 124 134 420 479 1505 1920 2078 1900 1447 851 386.91 548.10 533.86 432.87 236.73 164.96 154.02 864.73	266 55 40 269 04 02 259 25 19 257 26 10 39 52 01 258 39 20 251 13 52 261 43 22 262 45 49 40 262 16 49 263 17 40 264 47 45 265 07 18 267 23 267 280 23 279 37 42 280 259 19 261 43 22 262 16 49 263 12 19 264 47 45 31 38 58 26 26 47 45 279 32 15 104 18 32 12 10 256 23 267 280 225 280 259 37 41 280 256 19 49 40 29 40 20 26 46 49 20 26 33 21 15 22 22 240 23 25 32 24 41 25 26 33 26 33 27 28 36 41 28 37 42 29 46 41 29 40 2
WELL 3	693.84	262 17 36

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